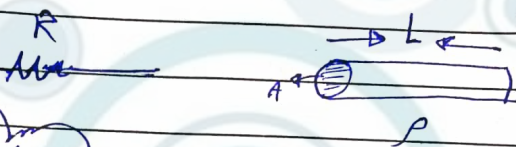


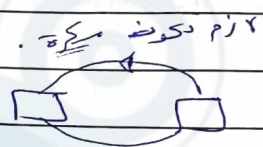
# Electrical:-

Resistor



$$R \propto \frac{L}{A}$$

$$R = \frac{\rho L}{A}$$

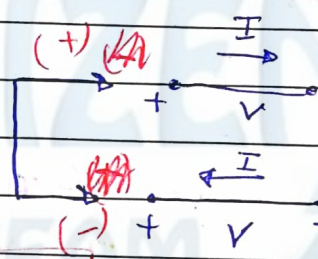
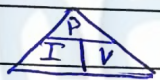


$$I = \frac{dQ}{dt} = \frac{\Delta Q}{\Delta t} \quad [A]$$

$$V_{\text{difference}} = V_{\oplus} - V_{\ominus}$$

$$P = IV$$

[W] watt



absorbed  
(consumed power)

consumed power

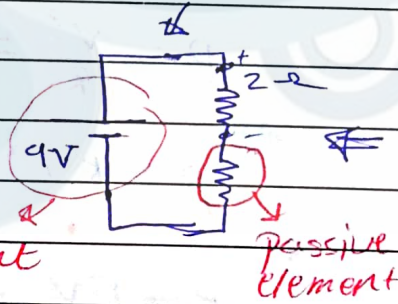
generated power

(Supplied power)

total power = zero

## Ohm's law:-

simplest circuit



active element

passive element

passive element

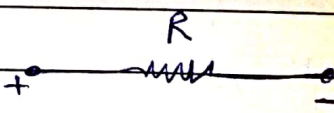
active element

(Voltage source)

supplies energy

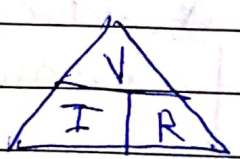
(Voltage source)

absorbs energy



$$V = IR$$

$$I = \frac{V}{R}$$



دائماً بينا اى اى اى  
للتيار دائل كالتالي

نوع التيار  
\$I\$



$$P_{\text{cons}} = IV = \frac{V^2}{R} = I^2 R$$

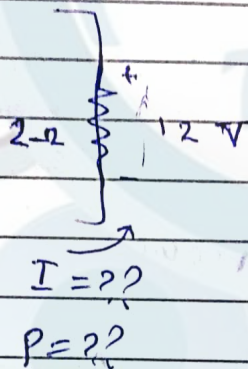
$$P_R \rightarrow \text{مقاومة} \rightarrow P_R = I_{ab} = -\text{sup}$$

### \* conductivity

$$G = \frac{1}{R} \quad (\text{S}, \overset{\text{mho}}{\leftarrow} \text{V}^{-1}, \rightarrow^{-1})$$

$$= \frac{I}{V} \quad \text{Siemens}$$

Ex:-



$$V = R \cdot I$$

$$I = \frac{V}{R} = \frac{12}{2} = -6 \text{ A}$$

كان التيار داخل البطارية

$$P = \frac{V^2}{R} = \frac{(12)^2}{2} = +72 \text{ W}$$

abs. power

$$P = R I^2 = (2)(-6)^2 = +72 \text{ W}$$

abs power

$$P = I V = (12)(-6) = -72 \text{ sup.}$$

$$= -72 \text{ sup.}$$

$$= +72 \text{ abs.}$$

\* Active element \*    المكون النشط

passive element    المكون السلبي

مصدر طاقة

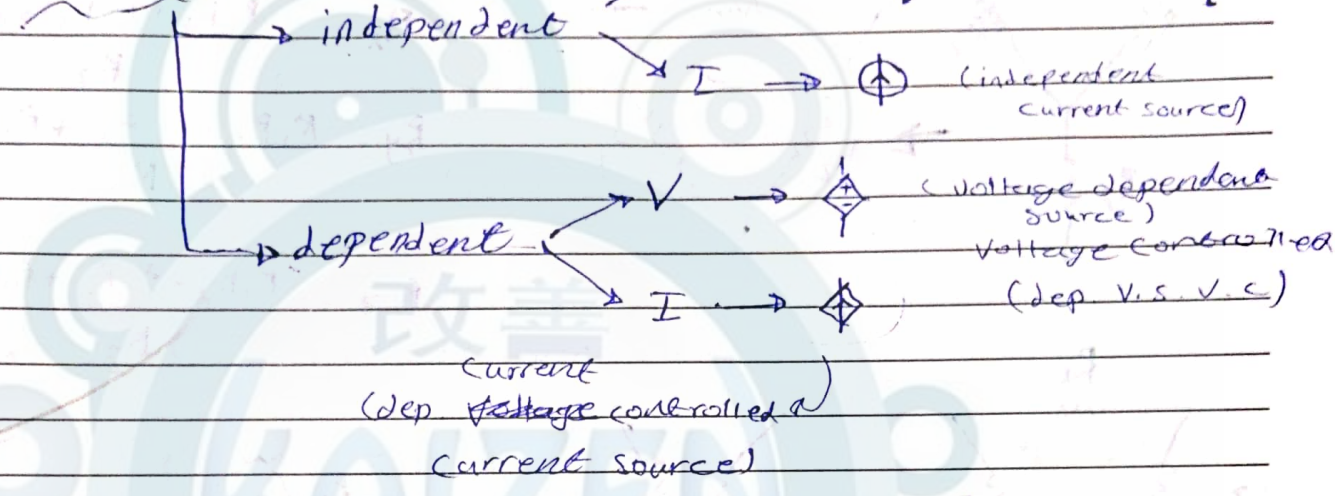
Source



توازي  
توازي  
توازي

التيار  
التيار  
التيار

\* Sources:-

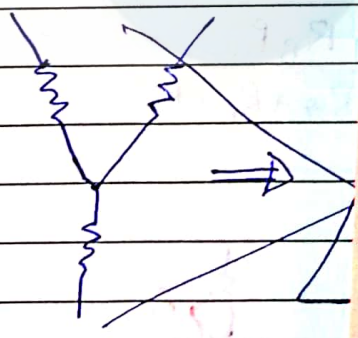


ip power u alast \*

\* Node -> wire one element

\* KCL  $\rightarrow \sum I_{in} = \sum I_{out}$  For every node

KVL  $\rightarrow \sum V = 0$  For every closed loop.



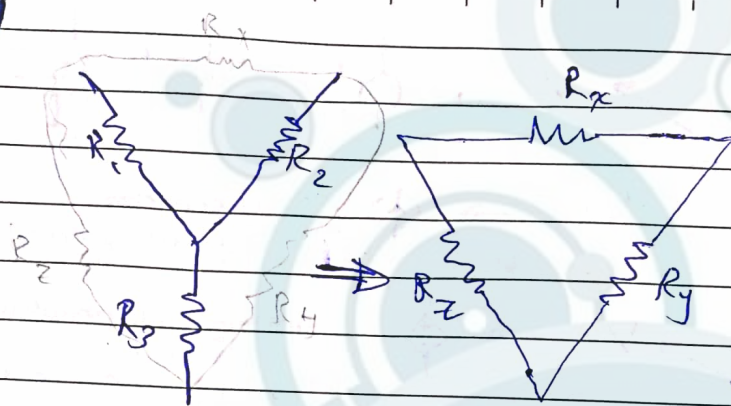
equivalent resistance

- Parallel  
  

$$\frac{1}{R_{eq}} = \frac{1}{R_1} + \frac{1}{R_2} + \dots + \frac{1}{R_n}$$
- Series  
  

$$R_{eq} = R_1 + R_2 + \dots + R_n$$
- other Form

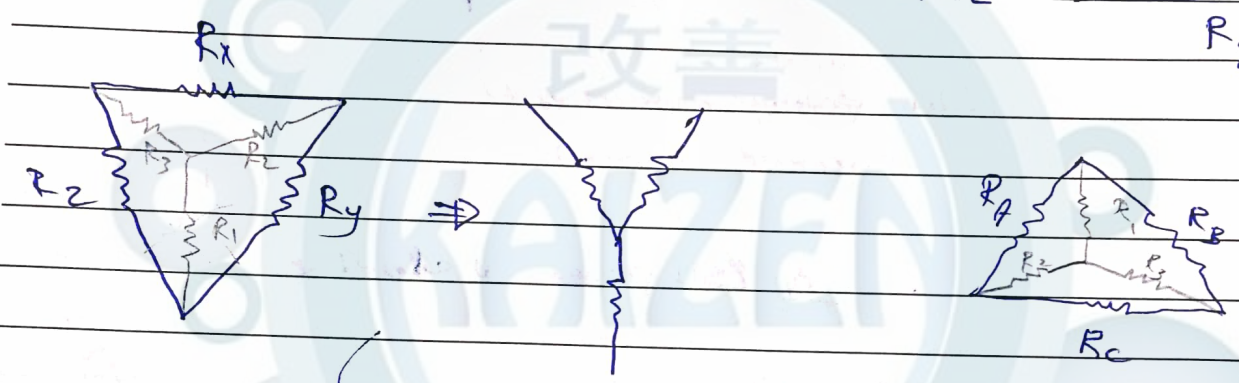




$$R_x = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_3}$$

$$R_y = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_1}$$

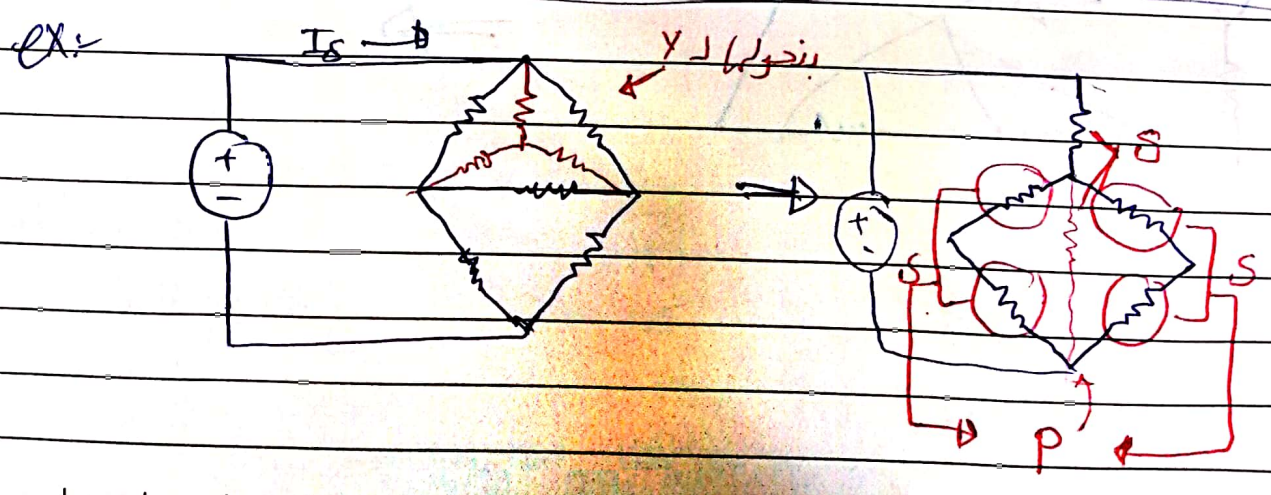
$$R_z = \frac{R_1 R_2 + R_2 R_3 + R_1 R_3}{R_2}$$



$$R_1 = \frac{R_A R_B}{R_A + R_B + R_C}$$

$$R_2 = \frac{R_A R_C}{R_A + R_B + R_C}$$

$$R_3 = \frac{R_B R_C}{R_A + R_B + R_C}$$





Rating power of R:-

$$P = I^2 R \quad (\text{allowed power})$$

انما كانت قدرة P اكثر من  
در allowed بكمي ابو  
damaged R, I

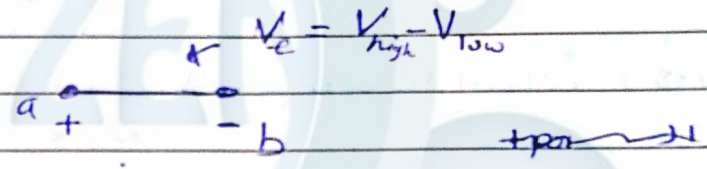
$$I_{max} = \sqrt{\frac{P_{max}}{R}} \quad (\text{allowed current})$$

\* Short circuit and open circuit:-

↳ wire is 0, 100%

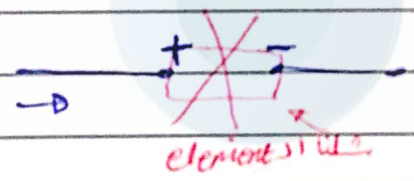
$$* R = 0$$

$$V = 0$$



Short circuit  $V_c = 0$  (+) polarity = (-) polarity  
 $V_+ = V_-$   
 $V_c = V_+ - V_- = 0$

open circuit



\*  $I = 0$  the current doesn't flow in an open part.  
 $R = \infty$

due to each other

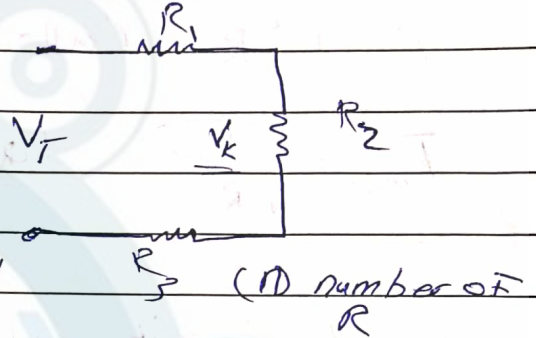
- $V \leftrightarrow I$
- $R \leftrightarrow G$
- $P \leftrightarrow S$  duality
- $\oplus \leftrightarrow \ominus$
- $S.C \leftrightarrow O.C$   
 $V=0 \quad V=0$



$$x = b - L + K$$

\* Voltage Division Rule :-

$$V_R = V_T \frac{R_K}{\sum_1^n R_i}$$



مثلاً  $\rightarrow V_2 = \frac{R_2}{R_1 + R_2 + R_3} \cdot V_T$

$$V_1 = \frac{R_1}{R_1 + R_2 + R_3} \cdot V_T$$

\* قواعد القسمة الجهدية

(series) كل المقاومات (R) متصلة في السلسلة  
كل المقاومات  $V_T$  متصلة في السلسلة

(Voltage sources) total

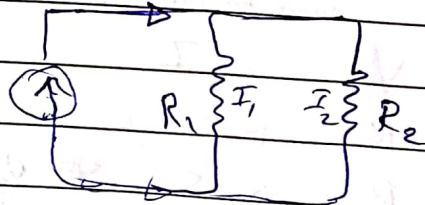
\* Current Division Rule :-

- ✓ Total current must be known
- ✓ all (R) are in parallel

$$I_R = \frac{R_n}{\frac{1}{R_1} + \frac{1}{R_2} + \dots + \frac{1}{R_n}} (I_{tot})$$

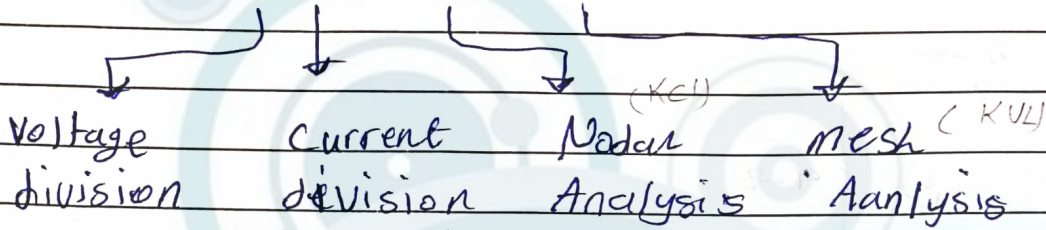
طريقة القسمة الجهدية

$$I_1 = \frac{R_2}{R_1 + R_2} I_{tot}$$





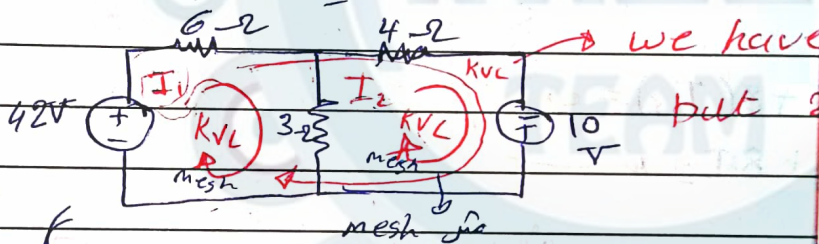
# Method of Analysis



## mesh analysis

every mesh is a KVL

لا بکونہ فیہا اکثر صونہ KVL



**\* Supernode:**  
 اذا كان غرضي 2 nodes بيناهم  
 voltage source  
 لا اجبر اهل في كافي في كل jump  
 node (مجانبة و بدو جرم مع بس)  
 بكتب (V2) و بجمع  
 او (V1)  
 $N(V2, V1) =$

meshes are given as clockwise.

$$-42 + V_6 + V_3 = 0 \rightarrow \text{mesh equation (1)}$$

$$6(I_1) + 3(I_1 - I_2) = 42$$

فار الی بکونہ الی انو mesh

$$N(2) \Rightarrow V_4 + (-10) + V_3 = 0$$

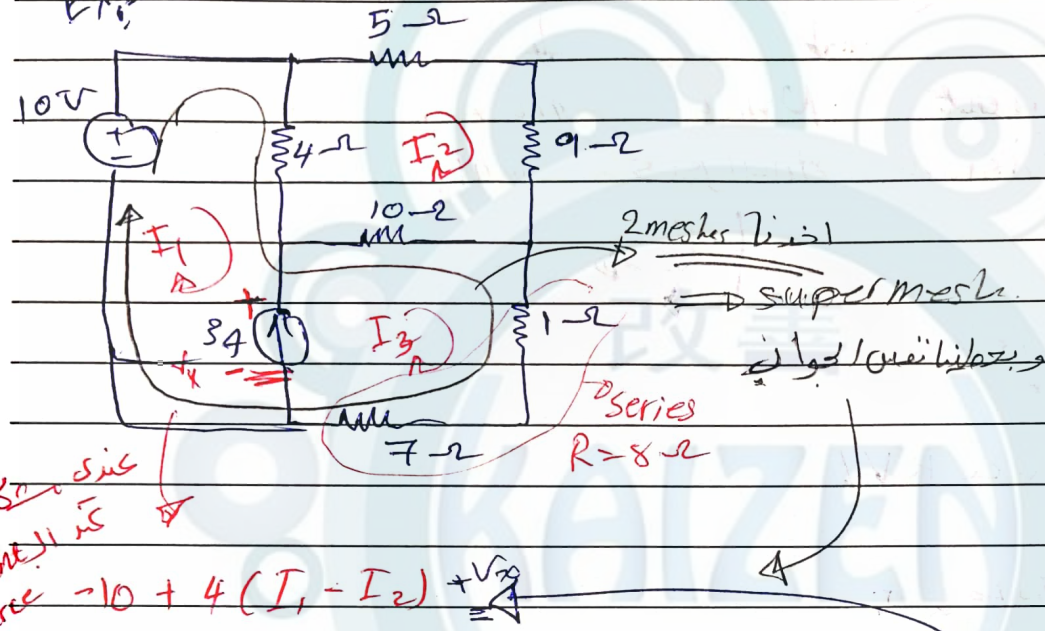
$$4(I_2) + 3(I_2 - I_1) = 10$$

meshes are given as clockwise.



# \* Supermesh:

Ex 11



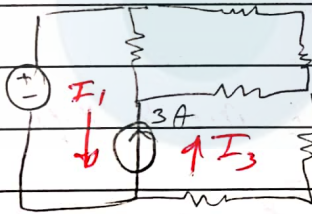
عند كسر الجهد  

$$-10 + 4(I_1 - I_2) + V_x = 0$$

KVL: 
$$-V_x + 10(I_3 - I_2) + 8(I_3) = 0$$

$$V_x = 10(I_3 - I_2) + 8(I_3)$$

S.M  $\Rightarrow 3 = I_3 - I_1$  --- (3)



$$\Rightarrow 3 = I_3 - I_1$$

$$-10 + 4(I_1 - I_2) + 10(I_3 - I_2) + 8(I_3) = 0$$
 --- (1)

$$4I_1 - 14I_2 + 10I_3 = 10$$
 --- (1)

$$10(I_2 - I_3) + 4(I_2 - I_1) + 5(I_2) + 9(I_2) = 0$$

$$-4I_1 + 28I_2 - 10I_3 = 0$$
 --- (2)

$$I_3 - I_1 = 3$$
 --- (3) 
$$I_3 = I_1 + 3$$

(1) + (2)  $\Rightarrow 14I_1 - 14I_2 + 10I_3 = 10$

$$-4I_1 + 28I_2 - 10I_3 = 0 \Rightarrow$$



$$\Rightarrow 14 I_2 = 10 \Rightarrow \boxed{I_2 = 0.7 \text{ A}}$$

$$4 I_1 - 14 I_2 + 10 I_3 = 10$$

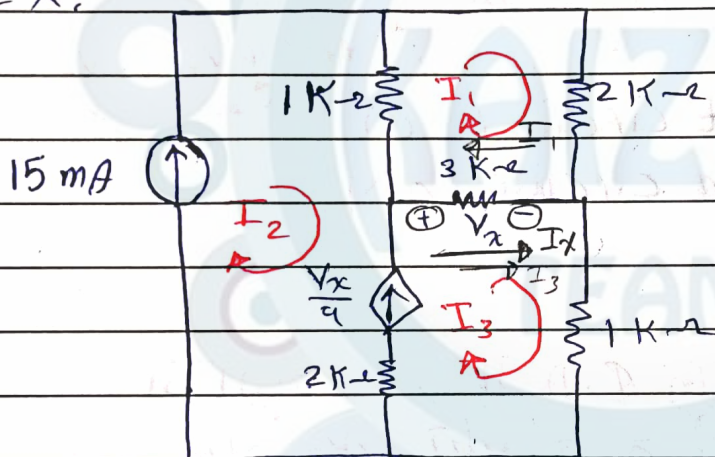
$$4 I_1 - 110 + 10(I_1 + 3) = 10$$

$$14 I_1 = 10 + 10 - 30$$

$$\boxed{I_1 = -2.5 \text{ A}}$$

$$\boxed{I_3 = 0.5 \text{ A}}$$

EX:



15 mA current source is given

15 mA

$$\boxed{I_2 = 15 \text{ mA}}$$

I.C.S.V.C in mesh (3)  $V_x = I_3 - I_2$

$$\text{but } \Rightarrow \frac{V_x}{9} = I_3 - I_2 \rightarrow 15$$

$$\frac{V_x}{9} = I_3 - 15 \quad \text{--- (1)}$$

$$\text{mesh (1)} \Rightarrow 1(I_1 - I_2) + 2(I_1) + 3(I_1 - I_3) = 0 \quad \text{--- (2)}$$

$$V_x = R_3(I_3 - I_1) \quad \text{--- (3)}$$

$$\Rightarrow V_x = 3(I_3 - I_1) \quad \text{--- (3)}$$

also  $R = 20 \text{ k}\Omega$



\* Superposition  $\rightarrow$  النظرية التراكبية

نظرية العناصر المستقلة

نظرية التيار  $i$

$$I = I' + I'' + I''' + \dots$$

$$V = V' + V'' + V''' + \dots$$

\* In order to get each individual contributor you have to kill all the other sources.

when we kill the

Voltage source  $\Rightarrow$  short circuit (S.C)

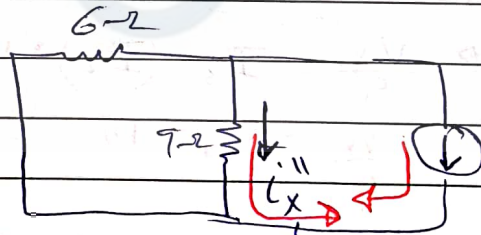
Current source  $\Rightarrow$  open circuit (O.C)

$$V = V_+ - V_-$$

$$0 = V_+ - V_- \Rightarrow V_+ = V_-$$

Killing the current source produces an open circuit

إذا أجبنا التيار، بال (O.C) يعاكس اتجاه التيار، إلى تيار أوجبه (i<sub>x</sub>)  
 راجع ~~نظرية~~ نظرية تيار  $i_x$  بال ~~نظرية~~ النظرية



التيار المضاف

when we have dependent source in the circuit don't kill it

بكل النظرية لا نرمز له

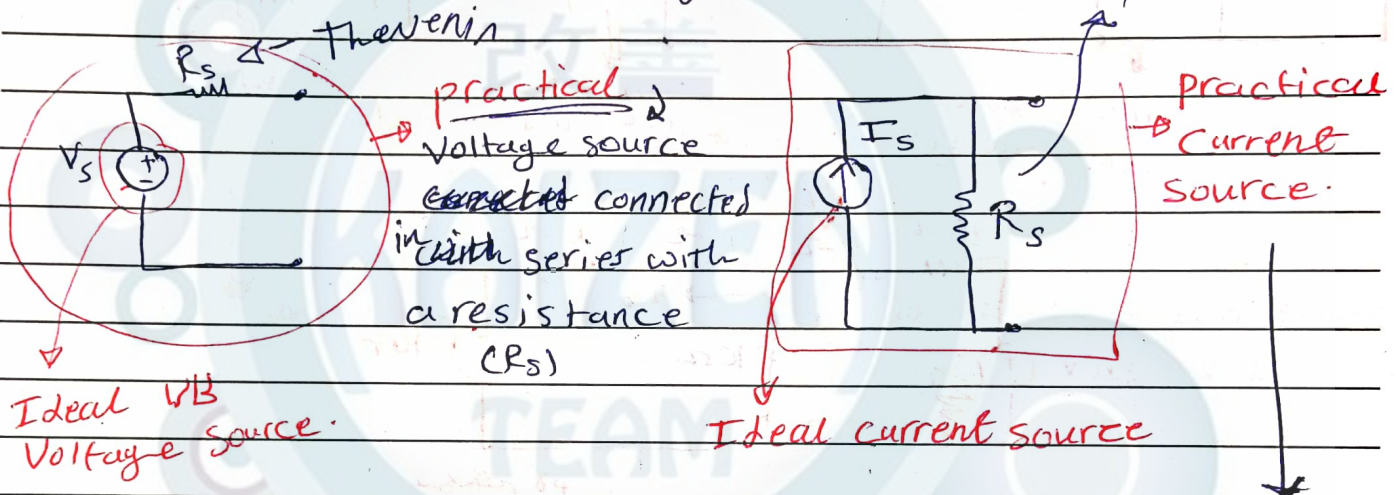


# \* Source Transformation:-

Ohm's law For suitable values.  $\Rightarrow$

There is a practical voltage source.

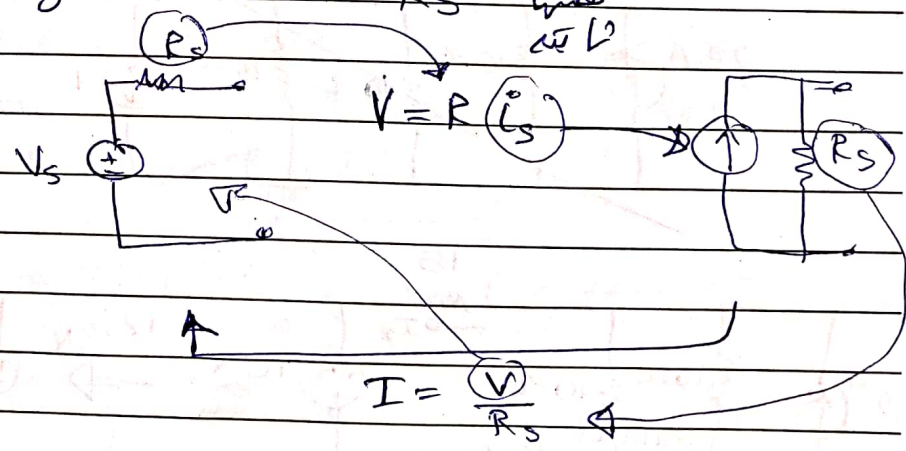
Norton:



Ideal current source connected in parallel with a resistance ( $R_s$ )

~~From~~ From practical current source to practical voltage source  $\Rightarrow R_s \rightarrow$   $\frac{V}{I}$

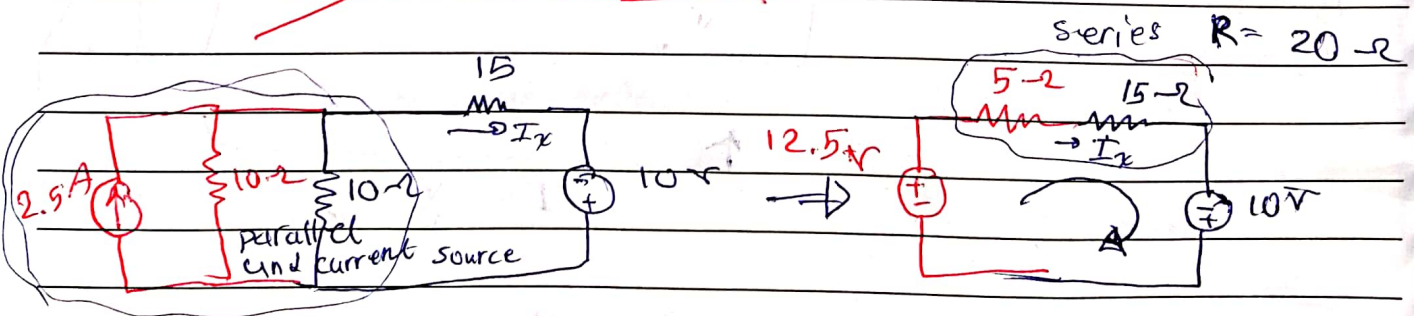
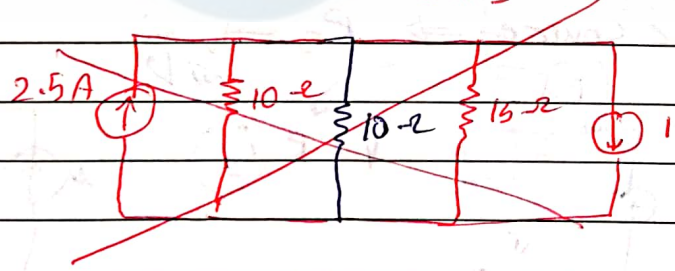
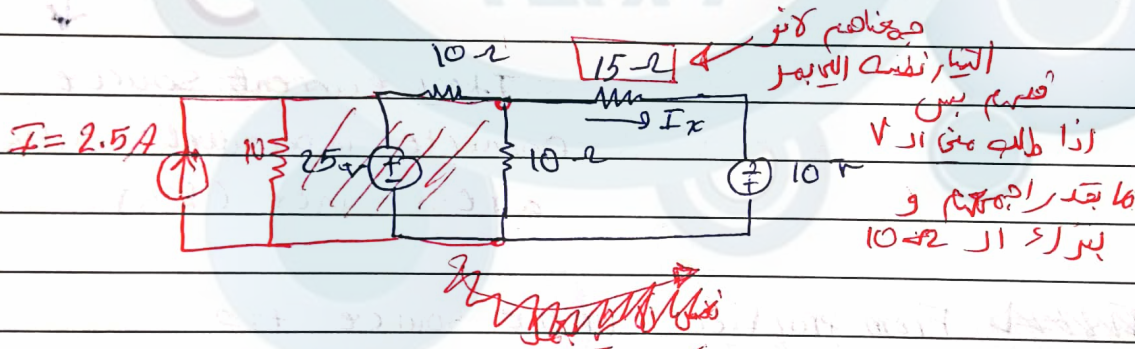
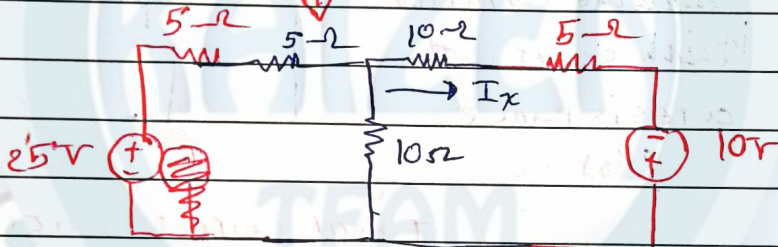
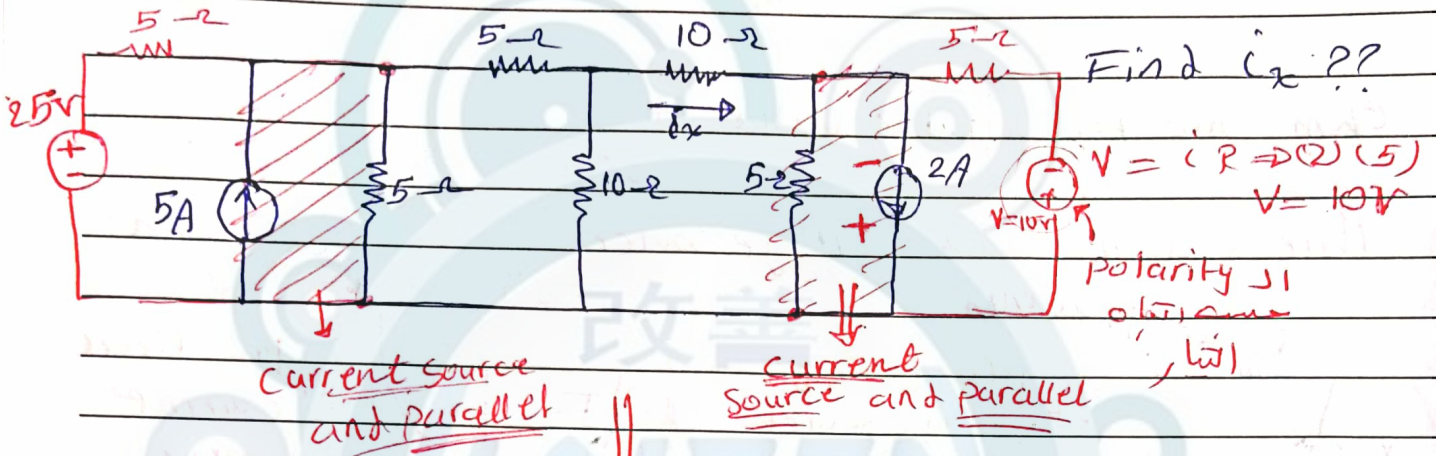
$R_s = R_s$   
 $V_s = I_s R_s$   
 $I_s = \frac{V_s}{R_s}$



التي  $I_s$   $\Rightarrow$   $\frac{V_s}{R_s}$   $\Rightarrow$   $\frac{V}{R_s}$   $\Rightarrow$   $I = \frac{V}{R_s}$



Ex-

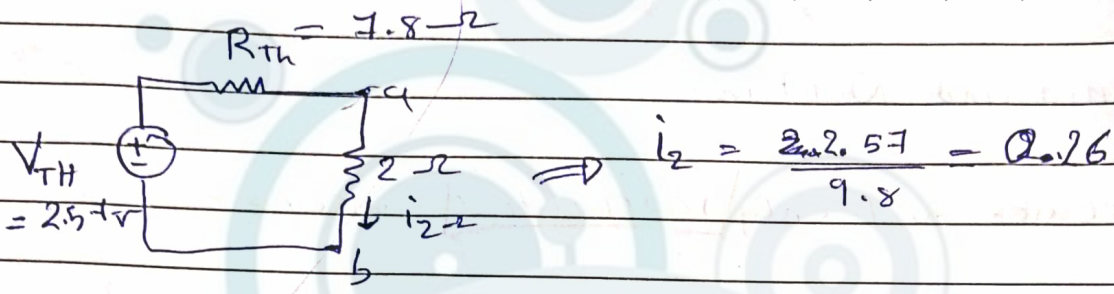


$$-12.5 - 10 + 20I_x = 0$$

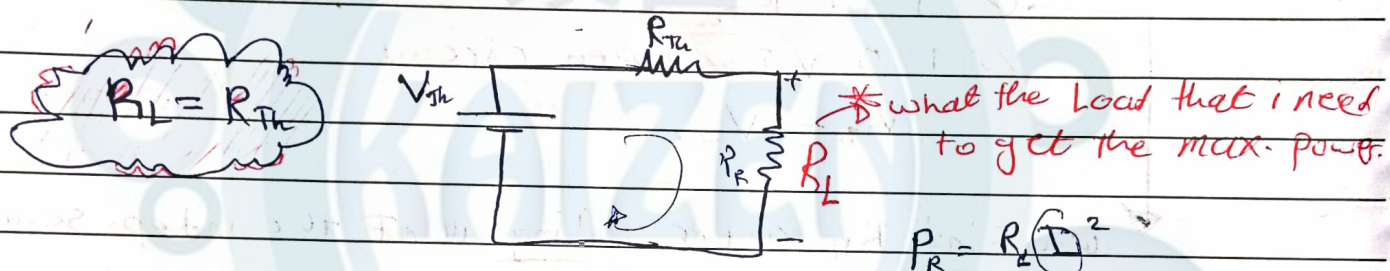
$$I_x = 1.125A$$







\* Maximum power Transferred.



$R_{TH} = 10$  اذا كان  $R_L = 7$

وذلك في  $P_{max}$  اذا كان  $R_L = R_{TH}$

what  $R_L$  to get the max power.

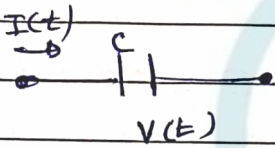
$$P_R = R_L \left( \frac{V_{TH}}{R_L + R_{TH}} \right)^2$$

$$P_{max} = \frac{V_{TH}^2}{4 R_{TH}} = \frac{I_{N}^2 R_{N}}{4}$$

transferred to load



## Capacitor :- (F)



$$I_c(t) = C \frac{dV(t)}{dt} \Rightarrow V_c(t) = \frac{1}{C} \int_{t_0}^t i_c(t) dt + \underbrace{V(t_0)}_{\text{Initial Condition}}$$

The capacitor in DC is represented by open circuit

← Joule

$$E = W = \frac{1}{2} C V^2 = \frac{1}{2} Q V = \frac{1}{2} \frac{Q^2}{C}$$

$$Q = CV$$

↑  
charge

$$C = \frac{1}{\frac{1}{C}} \downarrow V$$

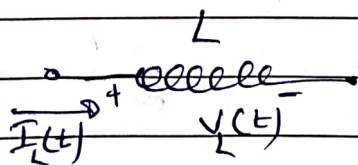
power =  $\frac{E}{t}$  ,  $P = IV$

capacitors in series  $\Rightarrow \frac{1}{C_{eq}} = \frac{1}{C_1} + \frac{1}{C_2} + \dots + \frac{1}{C_n}$

capacitors in parallel  $\Rightarrow C_{eq} = C_1 + C_2 + \dots + C_n$

}  $\omega SC$   
 $R$

## Inductor (#)



← Henry

duality  $\parallel$  in  $\rightarrow$  voltage  $\parallel$   $\rightarrow$  current

$$I_C(t) = C \frac{dV_C(t)}{dt}$$

$$\uparrow \quad \uparrow$$

$$V_L(t) = L \frac{di_L(t)}{dt}$$

duality

$$C \rightarrow L$$

$$I \rightarrow V$$

$$I_L(t) = \frac{1}{L} \int_{t_0}^t V_L(t) dt + i(t_0)$$

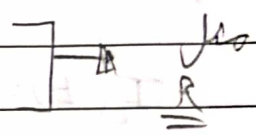
The inductor in DC circuite is represented by

Short circuit

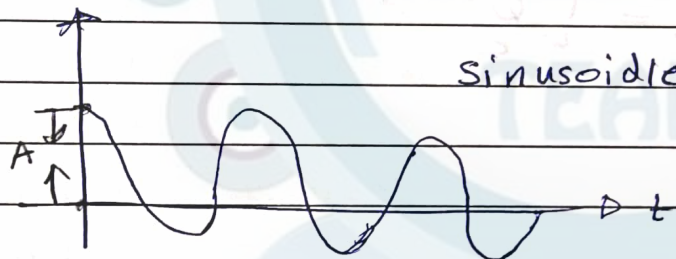
O.C  $\rightarrow$  S.C

inductor in **series**  $\Rightarrow L_{eq} = L_1 + L_2 + \dots + L_n$

inductor in **parallel**  $\Rightarrow \frac{1}{L_{eq}} = \frac{1}{L_1} + \frac{1}{L_2} + \dots + \frac{1}{L_n}$



\* Alternative current (AC)



sinusoidal wave

sinusoidal (average)  $\Rightarrow \frac{1}{\sqrt{2}}$

$x(t) = \frac{A}{\sqrt{2}} \cos(\omega t + \phi)$

Voltage  
Power  
Current

Amplitude  
 $V_m$   
 $I_m$

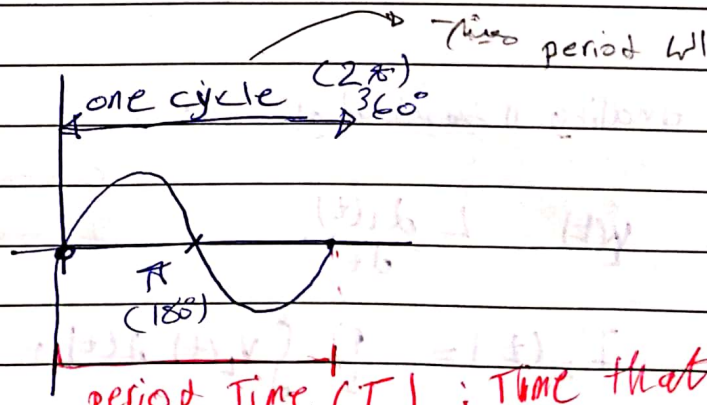
max value

phase shift (degrees or rad)

argument

angular Frequency (velocity)

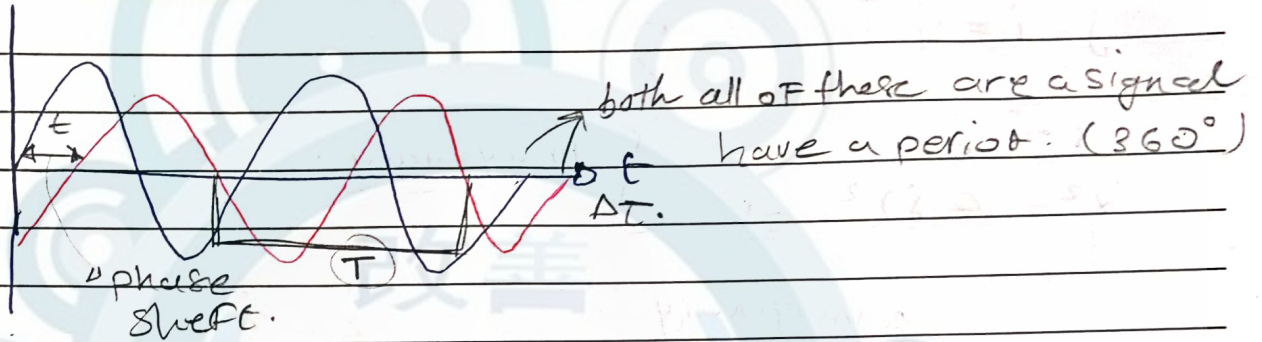
$\omega \rightarrow \frac{1}{s}$      $t \rightarrow s$



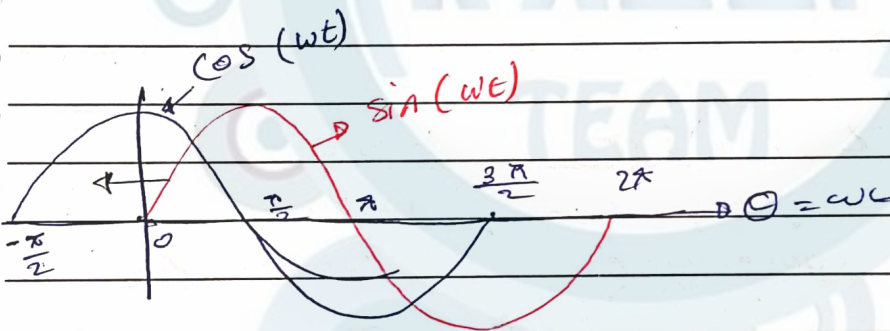
period Time (T) : Time that takes for a signal to make a one cycle.



~~scribble~~  $f = \frac{1}{T} \rightarrow \omega = 2\pi f \text{ (rad/s)}$



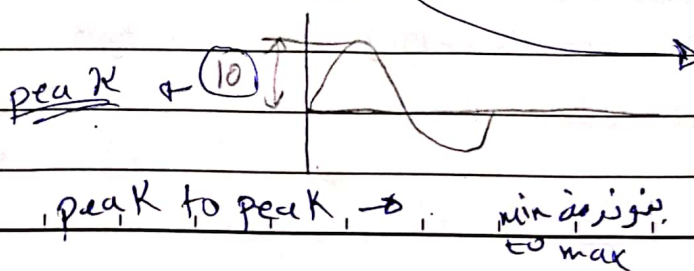
$$\theta = \frac{\Delta t}{T} \times \overset{\text{rad}}{2\pi} \text{ or } 360^\circ \text{ (degree)}$$



$$\sin(\omega t + 90^\circ) = \sin[\omega t + \frac{\pi}{2}] = \cos(\omega t)$$

sin is 90° ahead  
no shift w.r.t  
positive x-axis

Amplitude angular Frequency ( $\omega$ )  
 $10 \cos(377t + 30^\circ)$   
 phase shift ( $\theta$ )  
 Sinusoidal signal



$I(z, s)$   
 لا يا طو هو 2  
 له اعين ال 2  
 انتبه انوا ال اعين ال 2  
 و هو ال 2  
 Five Apple  
 ربيع

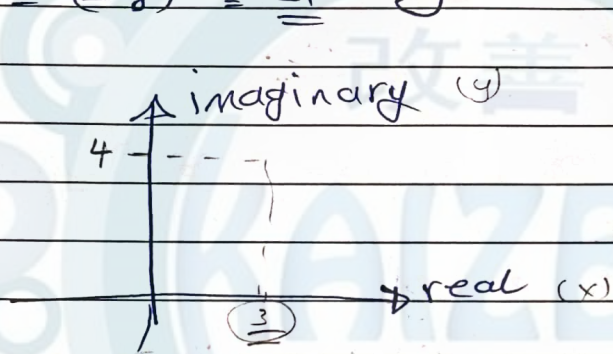
\* complex number:-

$$j = i = \sqrt{-1}$$

$$x = -j$$

$$x^2 = (-j)^2 = \underline{\underline{-1}}$$

} imaginary



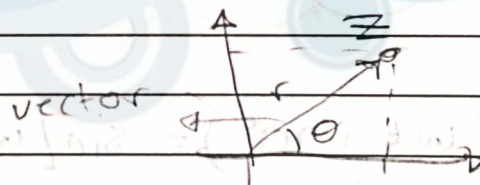
$$z_1 = \overset{\text{real}}{\downarrow} (3) + \overset{\text{imaginary}}{\downarrow} (4)j$$

in general  $\Rightarrow z = x + jy = r \angle \theta$

rectangular coordinate  $\Rightarrow$  Polar coordinate

$$* r = \sqrt{x^2 + y^2}$$

$$\theta = \tan^{-1}\left(\frac{y}{x}\right)$$



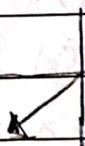
$$* x = r \cos \theta$$

$$y = r \sin \theta$$



180 + theta

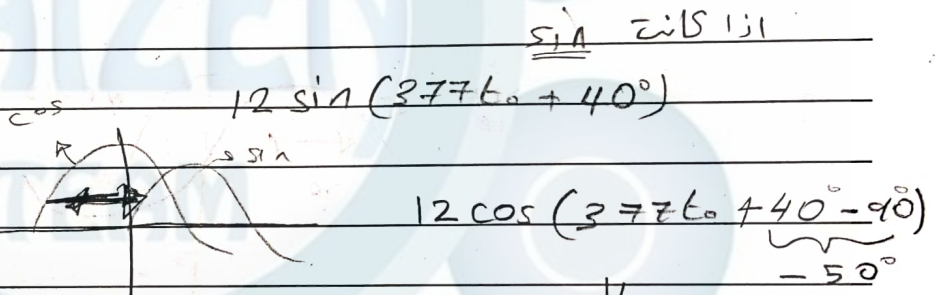
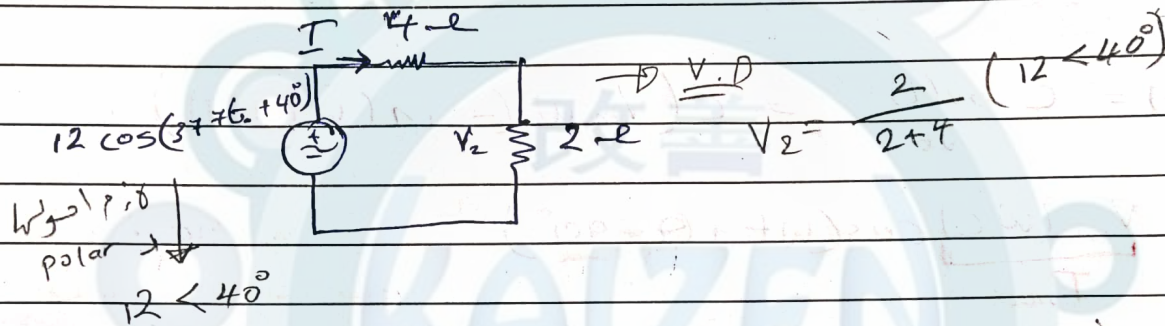
-180 + theta





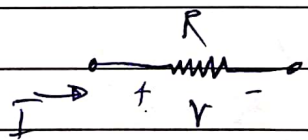
$$V(t) = \underset{V_m}{12} \cos(\underset{0}{377t} + 40^\circ)$$

$12 \angle 40^\circ \Rightarrow$  phasor form  $\rightarrow$  COS 11 22  
Frequency domain



$12 \angle -50^\circ$   
 $\sin(\omega t) = \cos(\omega t - 90)$   
 $\cos(\omega t) = \sin(\omega t + 90)$

### ① Resistor



$$V(t) = V_m \cos(\omega t + \theta)$$

$$I(t) = I_m \cos(\omega t + \theta)$$

$$V = IR$$

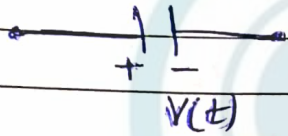
$$V(t) = V_m \angle \theta$$

$$I(t) = I_m \angle \theta$$

$$V_m \angle \theta = (I_m \angle \theta) R$$

I and V are in phase  
 (phase shift = 0)

② capacitor

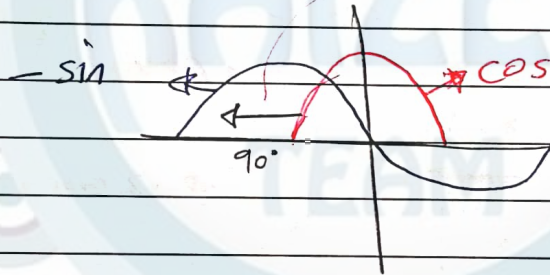


$$V(t) = V_m \cos(\omega t + \theta)$$

$$I(t) = C \frac{dV(t)}{dt} = C (V_m \omega (-\sin(\omega t + \theta)))$$

$$I(t) = \underbrace{V_m \omega C}_{I_{max}} \cos(\omega t + \theta + 90^\circ)$$

في فرق 90 درجة  
بين الـ sin والـ cos



$$V_c = V_m \angle \theta$$

$$I_c = I_m \angle \theta + 90^\circ$$

بزيادة 90 درجة

Voltage الـ 90 درجة

Impedance

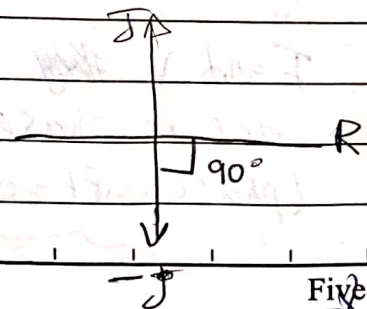
\* Impedance of capacitor (ohm)

$$X_c = \frac{V_c}{I_c} = \frac{V_m \angle \theta}{I_m \angle \theta + 90^\circ} \rightarrow (-j) \text{ bias}$$

$$= \left| \frac{V_m}{I_m} \right| \angle -90^\circ$$

↑  $I_m$   
↑  $V_c$

complexity is  $-jX_c$



Five Apple



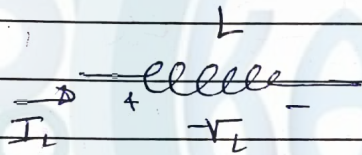
$$X_c = \frac{V_m}{I_{max}} = \frac{1}{\omega C}$$

$$\frac{V_m}{I_{max}}$$

$$Z_c = \frac{1}{j\omega C} = -j \left( \frac{1}{\omega C} \right) = -j X_c \quad (2)$$

Impedance plus sign is set & T is wrong

### ③ Inductor



$$V_L(t) = L \frac{di}{dt}$$

$$I_L(t) = I_m \cos(\omega t + \theta)$$

$$V_L(t) = I_m (\omega L) \cos(\omega t + \theta + 90^\circ)$$

horizontal  
quadrant

$$X_L = \frac{V_L}{I_L} = \frac{\omega L I_m \angle \theta + 90^\circ}{I_m \angle \theta} = \omega L \angle 90^\circ$$

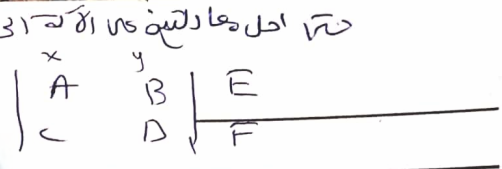
$$Z_L = +j\omega L = +j X_L \quad (3)$$

impedance plus sign

$R = \alpha$

$$x = \frac{ED - BF}{AD - BC}$$

$$y = \frac{AF - EC}{AD - BC}$$



\* Maximum Transferred power to load P ;  $L_{max}$

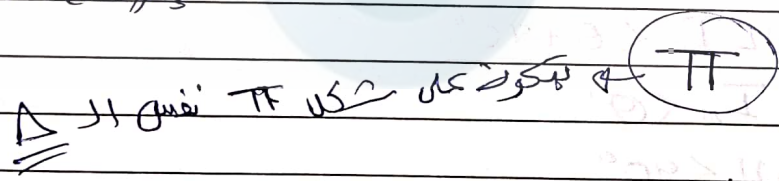
$$Z_L = Z_{Th}^*$$

conjugate (\*)  
 ↓  
 Change the sign of imaginary part  
 $4 + 3j \rightarrow 4 - 3j$

⊗ IF the sources didn't have a same ( $\omega$ )  
 we must use Superposition

phaser  
 آخرها بجزءه  
~~...~~

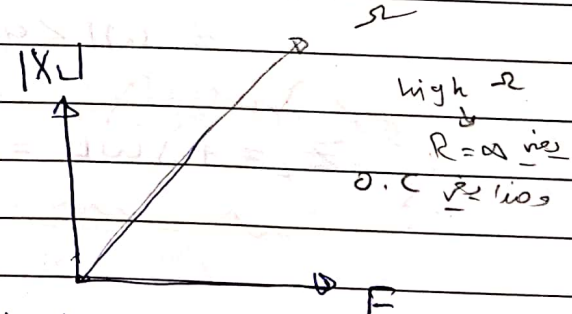
complex \*  
 not real #



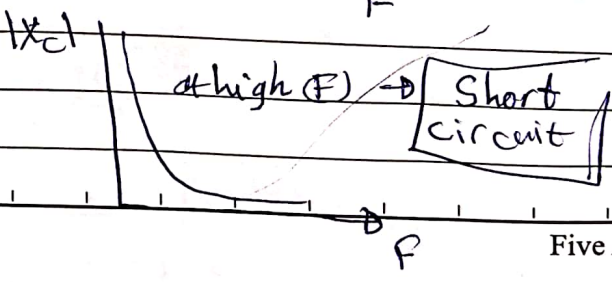
Frequency

$$* X_L = \omega L = 2\pi FL$$

(at high Freq  $\Rightarrow$  O.C)

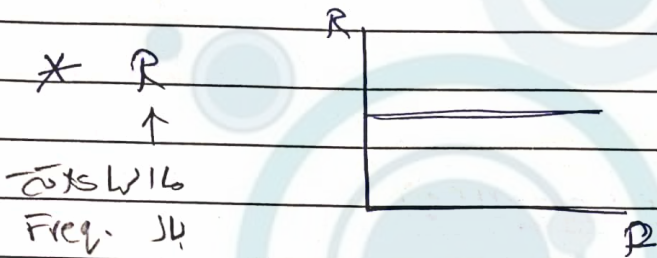


$$* X_C = \frac{1}{\omega C} = \frac{1}{2\pi FC}$$



...





$$Z = R + jX$$

\* R  
↑  
ω XL  
Freq. ↓

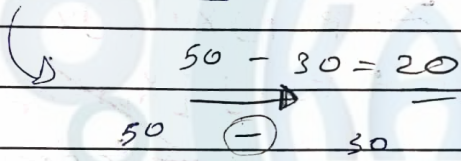
$$Z_R = R$$

↳ pure resistive

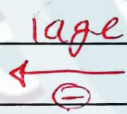
$$Z = +jX_L$$

⇒ pure inductive

$$Z = -jX_C \Rightarrow \text{pure capacitive}$$



i leads V



$$30 - 50 = -20$$

\* Admittance:

$$Y = G + jB$$

↑ conductance  
↳ susceptance

$$Z = R + jX$$

↑ resistance  
↑ reactance

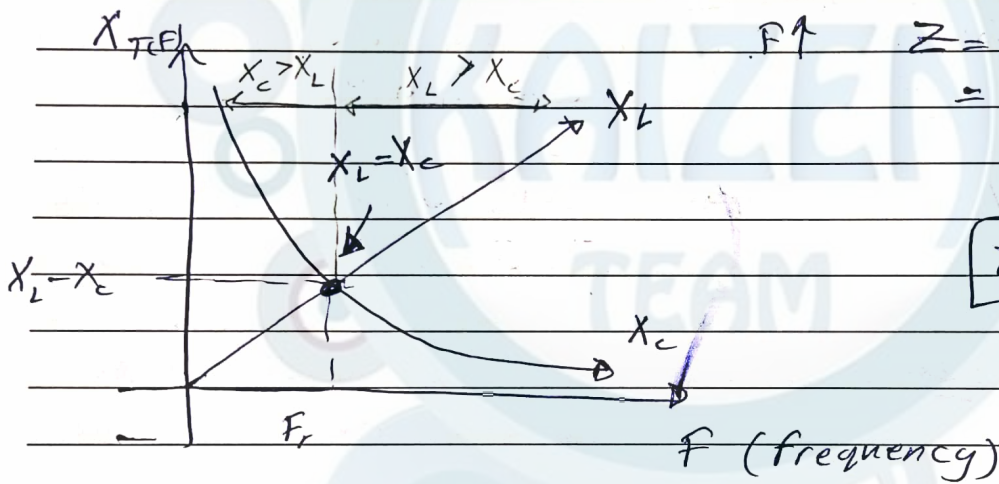
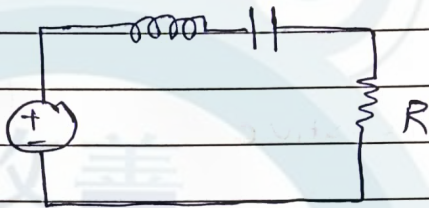
$$Y = \frac{1}{Z}$$

$$G = \frac{R}{Z}$$

$$B = -\frac{X}{Z}$$

# RLC Circuit

## \* Series RLC Circuit (series resonance)



$$Z = R + jX_L - jX_C$$

$$= R + j[X_L - X_C]$$

← zero

$Z = R$

$$Z = R + j \left[ \omega L - \frac{1}{\omega C} \right]$$

1. At high Frequencies:-

$$Z = R + jX$$

Inductive Behavior

2. At low Frequencies:-

$$Z = R - jX$$

capacitive behavior

3. At  $F = F_r$  ( $F_r$ )  $X_L = X_C$

$$\omega L = \frac{1}{\omega C}$$

Pure Resistive

$$Z = R$$

$$\theta = 0$$

$V_s$  and  $I_s$  are in phase



$$R_{MS} = \frac{I_{max}}{\sqrt{2}}$$

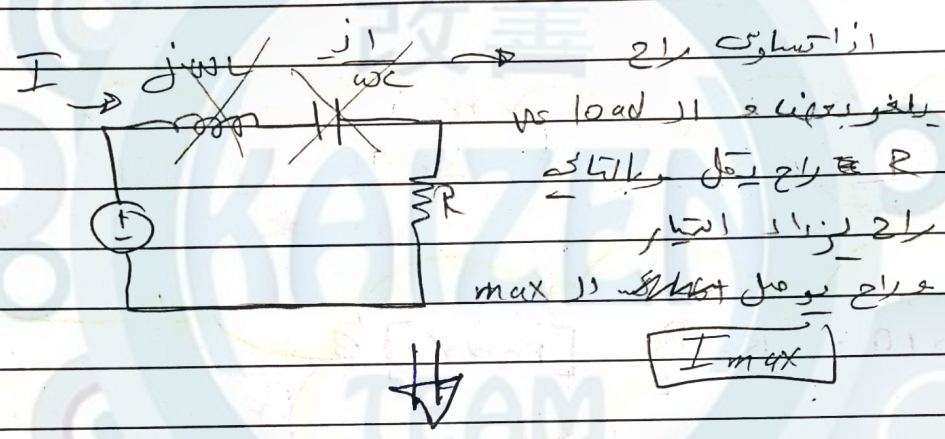
$$X_L = X_C$$

$$\omega L = \frac{1}{\omega C}$$

$$2\pi f L = \frac{1}{2\pi f C} \Rightarrow f = \frac{1}{2\pi\sqrt{LC}} \quad (\text{Hz})$$

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad (\text{rad/s})$$

resonance  
 $\Rightarrow$  Freq. ( $f_{res} = f_0$ )



$$|I| = I_{max}$$

$$R = R_s$$

$$V_L = I(jX_L) = IjX$$

$$V_C = I(-jX_C) = -IjX$$

$V_C$  will cancel  $V_L$

$$V_R = IR = R_s$$

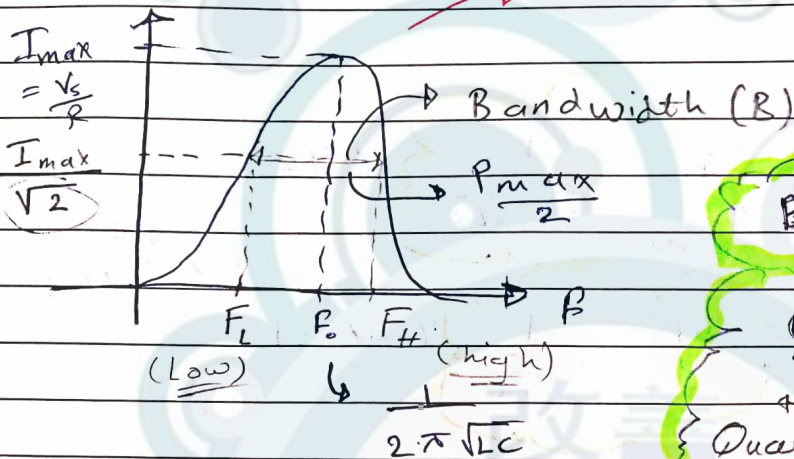
$$X_L = X_C \Rightarrow \omega L = \frac{1}{\omega C} \Rightarrow Z_{min} = R$$

$$I_{max} = \frac{V_{supply}}{R}$$

$$\omega L = \frac{1}{\omega C} \Rightarrow \omega^2 = \frac{1}{LC} \Rightarrow \omega = \frac{1}{\sqrt{LC}}$$



$$I_{\text{max}} = \frac{I_{\text{max}} T}{\sqrt{2}}$$



$$B = f_H - f_L \quad B = \frac{R}{L}$$

$$Q = \frac{R}{B} = \frac{1}{R} \sqrt{\frac{L}{C}}$$

Quality Factor.

$$P_{\text{max}} = I_{\text{max}} R \Rightarrow \frac{P_{\text{max}}}{2} = \frac{I_{\text{max}}^2 R}{2}$$

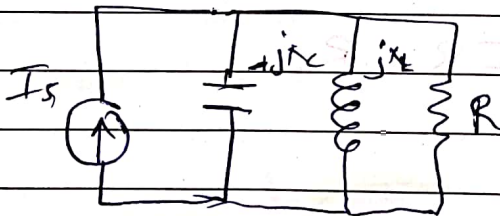
$$* \text{ If } Q > 10 : B = \frac{R}{L} \text{ [rad/s]}$$

$$Q = \frac{\omega_0 L}{R} \text{ (rad/s)}$$

$$f_{\text{low}} = f_0 - \frac{B}{2}$$

$$f_{\text{high}} = f_0 + \frac{B}{2}$$

### \* Parallel RLC Circuit :-



$$X_L = X_C$$

$$\omega L = \frac{1}{\omega C}$$

$$f_0 = \frac{1}{2\pi\sqrt{LC}} \text{ (Hz)}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$



$$P = \frac{V_{rms}}{|Z|} \cos \phi$$

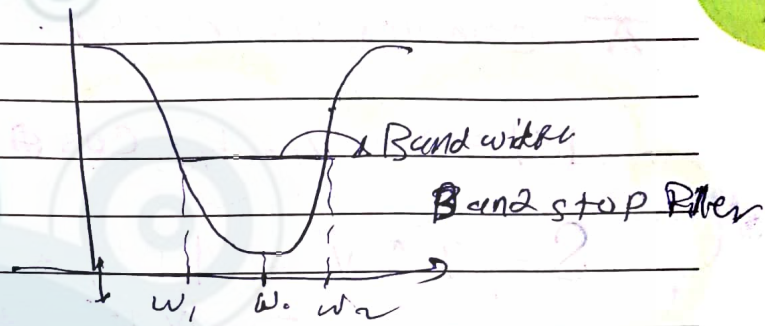
$$\frac{P}{|S|} = P.F. = \frac{\cos \phi}{P.F.}$$

$$T = \frac{2\pi}{\omega}$$

$\phi = \theta_v - \theta_i$

$$Z = R_{max}$$

$$I_{min} = \frac{V}{R}$$



$$* B = \omega_2 - \omega_1 = \frac{1}{RC}$$

$$Q = \frac{f_0}{B}$$

$$* \omega_0 = \sqrt{\omega_1 \omega_2}$$

$$f_H = f_0 + \frac{1}{2} B$$

$$f_L = f_0 - \frac{1}{2} B$$

$$Q > 10 \rightarrow \omega_1, \omega_2 = \omega_0 \pm \frac{B}{2}$$

$$Q = \frac{\omega_0}{B} = \frac{f_0}{B}$$

### \* effective value (RMS)

$X_{RMS} = \text{DC value for DC}$

$$\tilde{V} = V_{rms} = \begin{cases} \frac{V_m}{\sqrt{2}} & \text{sinusoidal} \end{cases}$$

$$P_{avg} = I \cdot \tilde{V}$$

$$X_{rms} = \frac{X_m}{\sqrt{2}}$$

for sinusoidal only

$$V_m \quad \text{square}$$

$$\frac{V_m}{\sqrt{3}} \quad \text{triangle}$$

$$V(t) = V_1 \cos(\omega t + \theta) + V_2 \cos(\omega t) + V_3 \sin(\omega t + \theta) + \dots + V_n$$

$$V_{rms} = \sqrt{V_1^2 + \sum \frac{V_i^2}{2}}$$



$$I_{rms} \cos \theta \text{ p.u.} \rightarrow \cos \theta = \frac{P}{S}$$

$$\hookrightarrow P = I_{rms} V_{rms} \cos(\theta_v - \theta_i)$$

\* complex power (S)

$$|S| = S = V_{rms} I_{rms} \cos \theta$$

$$S = \tilde{I}^* \tilde{V} = |\tilde{I}|^2 Z$$

$$= \frac{|\tilde{V}|^2}{Z^*}$$

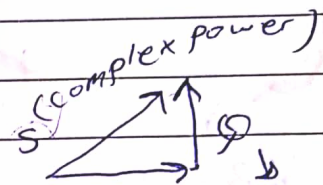
$$P = |S| \cos \theta = I_{rms}^2 R = \frac{V_{rms}^2}{R}$$

$$Q = |S| \sin \theta = I_{rms}^2 X = \frac{V_{rms}^2}{X}$$

↳ reactive power

↳ dissipated power

~~XXXXXXXXXX~~



$$|Z| = \sqrt{R^2 + X^2}$$

$$Z = R + jX$$

$$S = \sqrt{P^2 + Q^2}$$

$$S = P + jQ$$

power factor (PF) =  $\cos \theta = \frac{P}{|S|}$

\* instantaneous power:-

$$p(t) = v(t) \cdot i(t)$$

$$= V_m \cos(\omega t + \theta_v) \cdot I_m \cos(\omega t + \theta_i)$$

$$= \frac{V_m I_m}{2} [\cos(2\omega t + \theta_i + \theta_v) + \cos(\theta_v - \theta_i)]$$

$$p(t) = \underbrace{\frac{1}{2} I_m V_m \cos(\theta_v - \theta_i)}_{\text{DC-term}} + \frac{1}{2} I_m V_m \cos(2\omega t + \theta_i + \theta_v)$$

DC term  $\rightarrow$  average, Real, Active power



reactive power  $\rightarrow (\Theta)$

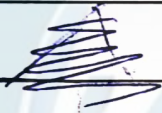
$$Q = \frac{1}{2} I_m V_m \sin(\Theta_v - \Theta_i)$$

$\sin 0 = 0 \rightarrow R \text{ voltage } \rightarrow Q \rightarrow 0$

$Q \rightarrow L (+) V$

$Q \rightarrow C (-) V$

$Q \rightarrow R X$



$|S| < \Theta_s$

↑  
apparent power

$S = P + jQ$

زاویه  $\Theta$

جریان  
p.f.  $\sin$

$P.F. = \cos \Theta$   
 $= \cos(\Theta_v - \Theta_i)$

$\Theta \rightarrow L (+)$

$\Theta \rightarrow C (-)$

$S = V_{rms} \cdot I_{rms}^*$

$I = |I| < \Theta$

$I^* = |I| < -\Theta$

① instantaneous power :-

$$P(t) = V(t) \cdot i(t)$$

$$= V_m \cos(\omega t + \theta_v) * I_m \cos(\omega t + \theta_i)$$

$$= \frac{V_m I_m}{2} \cos(2\omega t + \theta_i + \theta_v) + \frac{V_m I_m}{2} \cos(\theta_v - \theta_i)$$

② Avg. power :-

$$P_{avg} = \frac{V_m I_m}{2} \cos(\theta_v - \theta_i)$$

از ایا  
ارتباط

$$\Rightarrow P_{avg} = \frac{1}{2} I_m^2 |Z| \cos(\theta_v - \theta_i)$$

$$= \frac{1}{2} \frac{V_m^2}{|Z|} \cos(\theta_v - \theta_i)$$

$$Z_{total} = r \angle \theta$$

$$\theta_{total} = \theta_v - \theta_i$$

rms

$$\Rightarrow P_{avg} = V_{rms} I_{rms} \cos(\theta_v - \theta_i)$$

$$= I_{rms}^2 |Z| \cos(\theta_v - \theta_i)$$

$$= \frac{V_{rms}^2}{|Z|} \cos(\theta_v - \theta_i)$$

③ complex power :-

$$S = V_{rms} I_{rms}^* = P + jQ$$

$$P = V_{rms} I_{rms} \cos(\theta_v - \theta_i)$$

$$Q = V_{rms} I_{rms} \sin(\theta_v - \theta_i)$$

Summary

$$S = V_{rms} I_{rms}^* = V_{rms} I_{rms} \cos(\theta_v - \theta_i) + j V_{rms} I_{rms} \sin(\theta_v - \theta_i)$$

$$= \underbrace{|I_{rms}|^2 R}_P + j \underbrace{|I_{rms}|^2 X}_Q$$



dissipated power  
 $\rightarrow I_{rms}^2 R$

Complex power  
 $= P_{total} + jQ_{total}$

④ Power Factor

$PF = \cos(\theta_v - \theta_i)$

$PF = \frac{P}{V_{rms} I_{rms}} = \frac{P}{|S|}$       $|S| = \sqrt{P^2 + Q^2}$

Case for PF  $\Rightarrow$  ①  $PF = 1 \Rightarrow$  pure resistive load

$\theta_v = \theta_i$  ,  $\cos(\theta_v - \theta_i) = \cos 0 = 1$   
 $\sin(\theta_v - \theta_i) = 0$   
 $\Rightarrow Q = 0$

②  $PF = 0 \Rightarrow$  pure inductive load.

$Q > 0$   $PF = \cos \theta = \cos 90 = 0$

$PF = 0$   $\cos(\theta_v - \theta_i) = \cos 90 = 0$

$\Rightarrow$  pure capacitive load.

$Q < 0$

$PF = \cos(\theta_v - \theta_i) = \cos(90) = 0$

③ inductive load PF  $\rightarrow$  lagging

ex:  $PF = 0.8$  lag

capacitive load PF  $\rightarrow$  leading

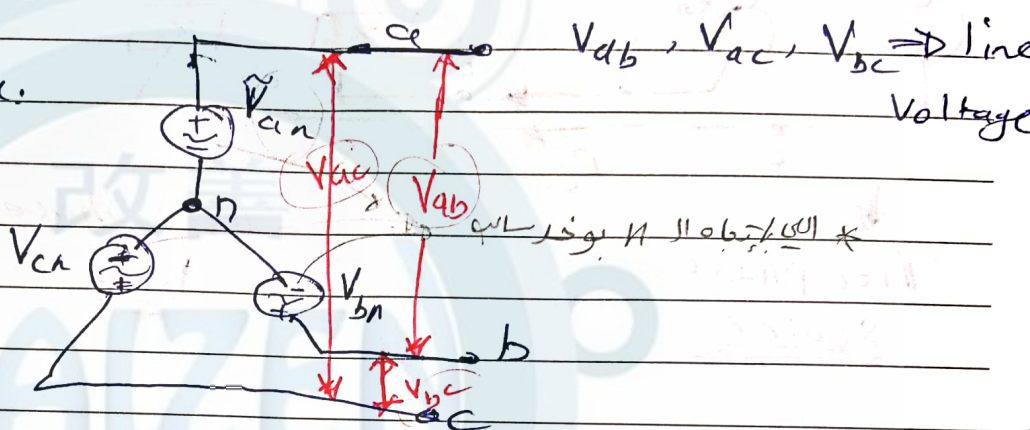
$|S| = 1000$  VA

$S = |S| \angle \theta = \cos^{-1}(PF)$   
 inductive load

### 3-phase system:-

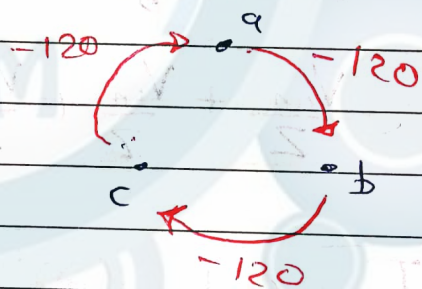
Source	load
Y	Y
Y	$\Delta$

Y configuration:



n: Neutral node

$$\left. \begin{aligned} \underline{V_{an}} &= V \angle 0^\circ \\ \underline{V_{bn}} &= V \angle -120^\circ \\ \underline{V_{cn}} &= V \angle -240^\circ \end{aligned} \right\}$$



phase shift  
 $\theta = 120^\circ$

phase Voltages

$$\underline{V_{an}} + \underline{V_{bn}} + \underline{V_{cn}} = 0$$

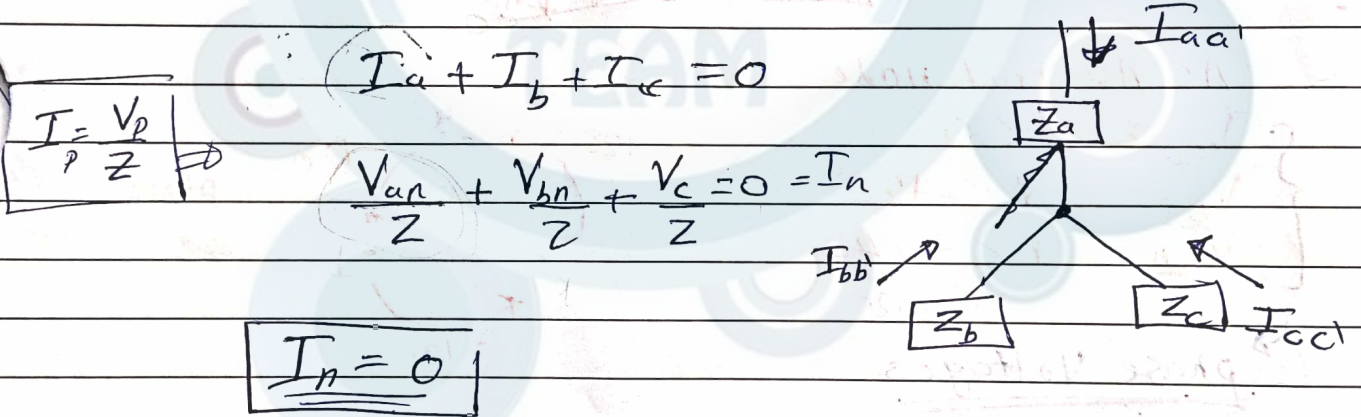
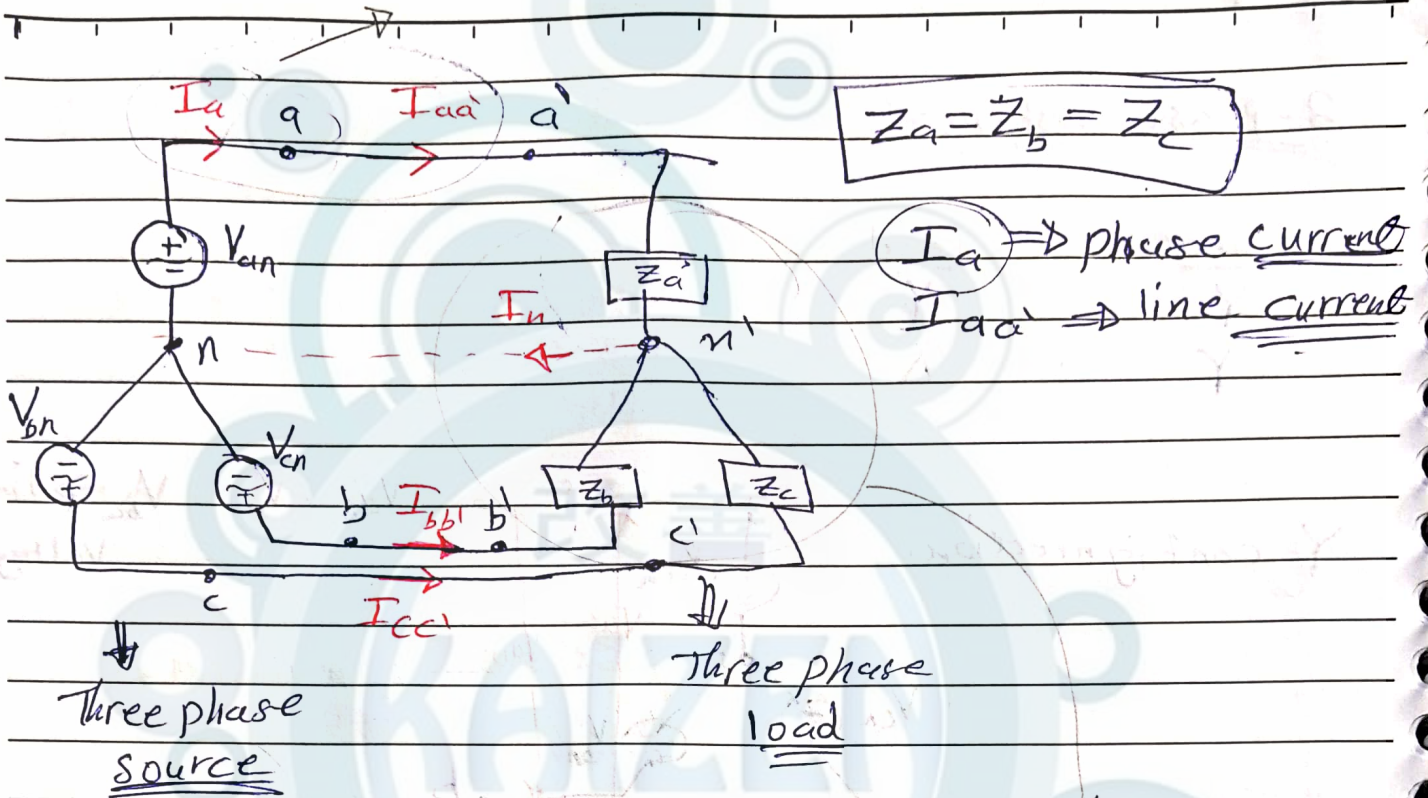
line voltages  $\Rightarrow V_{ab} = V_{an} - V_{bn}$

$$\left. \begin{aligned} V_{ab} &= \sqrt{3} V_{an} < 30 \\ V_{bc} &= \sqrt{3} V_{bn} < 30 \\ V_{ca} &= \sqrt{3} V_{cn} < 30 \end{aligned} \right\}$$

$\Rightarrow$  They are equal to  $\sqrt{3} V_n < 30$

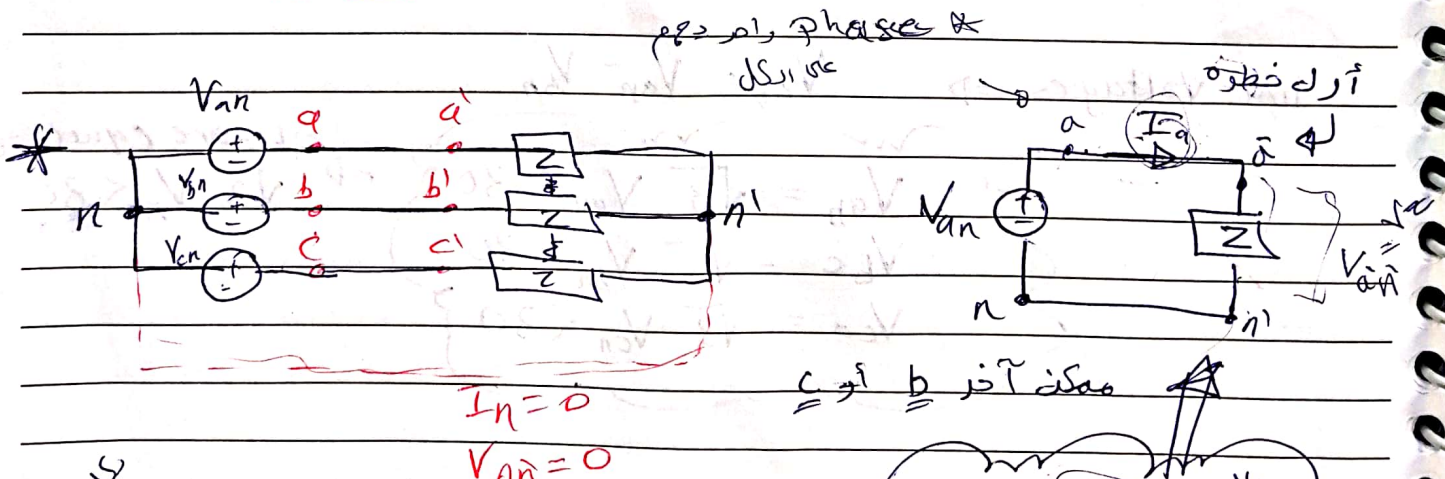


$$I_{\text{phase}} = I_{\text{line}} \sqrt{3}$$



Current in the wire between n, n' = 0

$$V_{nn'} = 0$$

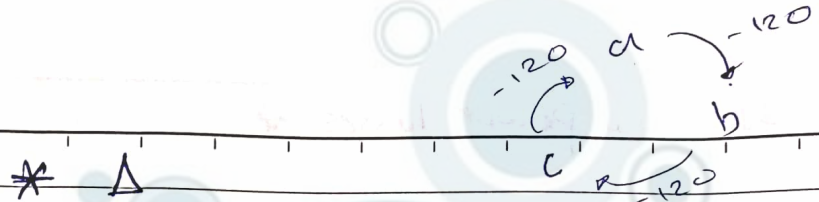


3 phases

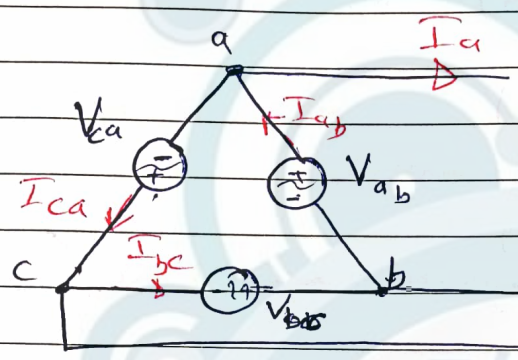
$$S_{\text{load (total)}} = 3 * \text{[Symbol]}$$

$$S_{\text{load}} = V_{an} I_a^*$$





$I_a, I_b, I_c \rightarrow$  line current  
 $V_{ab}, V_{bc}, V_{ca} \rightarrow$  phase voltage



$I_{ab} \neq I_a$   
 $V_{phase} = V_{line}$

$$\begin{aligned}
 I_a &= \sqrt{3} I_{ab} \angle -30^\circ \\
 I_b &= \sqrt{3} I_{bc} \angle -30^\circ \\
 I_c &= \sqrt{3} I_{ca} \angle -30^\circ
 \end{aligned}$$

$$I_{ab} = \frac{I_a}{\sqrt{3}} \angle -30^\circ$$

$$I_{bc} = \frac{I_b}{\sqrt{3}} \angle -30^\circ$$

$$I_{ca} = \frac{I_c}{\sqrt{3}} \angle -30^\circ$$

\* power in 3-phase system:-

$$\begin{aligned}
 S_{total} &= 3 V_{phase} * I_{phase}^* \\
 &= \sqrt{3} V_{line} * I_{line}^* \\
 &= P_{total} + j Q_{total}
 \end{aligned}$$

$$\begin{aligned}
 P_{total} &= 3 V_{phase} I_{phase} \cos(\theta_v - \theta_i) \\
 &= \sqrt{3} V_{line} I_{line} \cos(\theta_v - \theta_i) \Rightarrow
 \end{aligned}$$



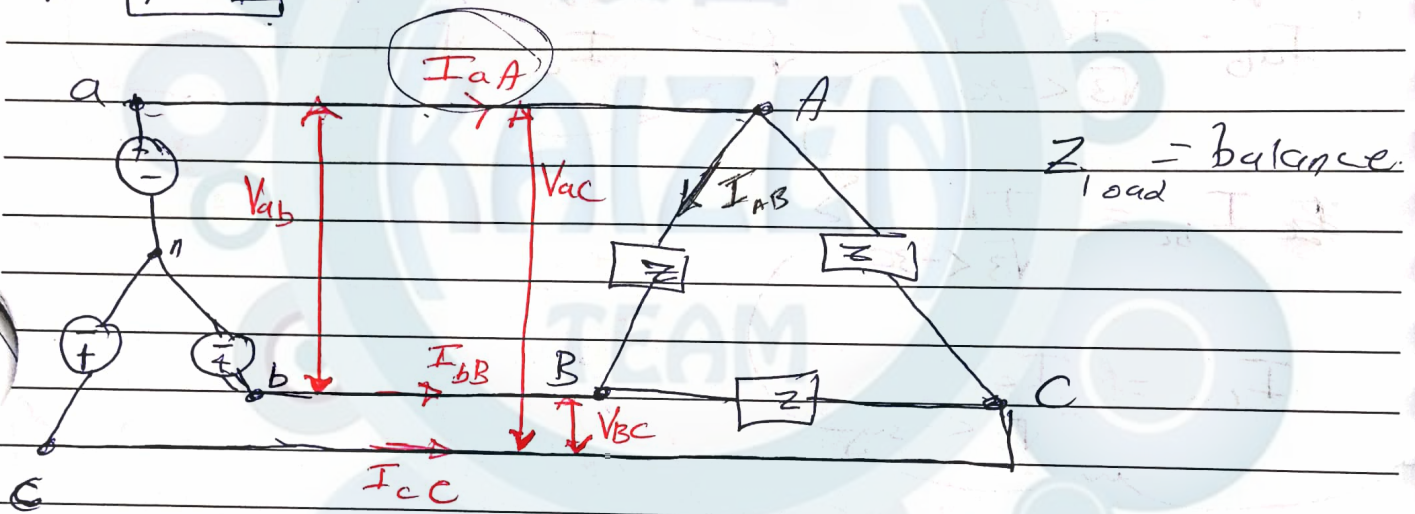
R تىرىشچانلىقى power losses \*

$$P = 3 V_{\text{phase}} I_{\text{phase}} \sin(\theta_v - \theta_i)$$

$$= \sqrt{3} V_{\text{line}} I_{\text{line}} \sin(\theta_v - \theta_i)$$

$$PF = \cos(\theta_v - \theta_i) \rightarrow \begin{cases} \text{leading} \\ \text{lagging} \end{cases}$$

\*  $\Delta - Y$  ~~em~~



$$V_{AB} = V_{ab}, \quad I_{AB} = \frac{V_{ab}}{Z} = \frac{\sqrt{3} V_{an} \angle 90^\circ}{Z}$$

$$I_{BC} = \frac{V_{bc}}{Z} = \frac{\sqrt{3} V_{bn} \angle 30^\circ}{Z}$$

$$I_{CA} = \frac{V_{ca}}{Z} = \frac{\sqrt{3} V_{cn} \angle -30^\circ}{Z}$$

$$I_{aA} = \sqrt{3} I_{AB} \angle -30^\circ$$


$$Z = \frac{Z \times Z}{3Z}$$

\*  $\Delta - Y$  تىرىشچانلىقى تىرىشچانلىقى

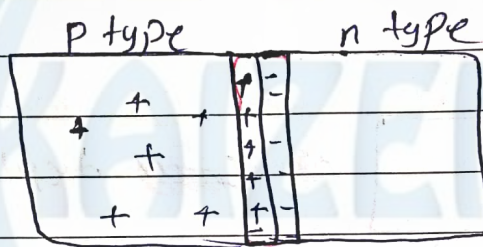
Germanium

# \* Semiconductor - Devices: Si, Ge

Semiconductor are materials having electrical properties between conducting & insulating material.

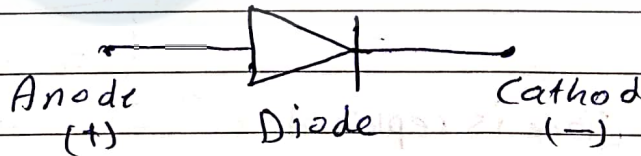
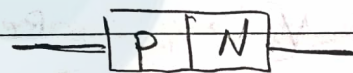
 n-type semi cond. : majority is electron (-ve) sign

 p-type semi cond. : majority is hole (+ve) sign



depletion region

$V_g \rightarrow (0.6 - 0.7) \rightarrow Si$   
 $\rightarrow (0.2 - 0.3) \rightarrow Ge$

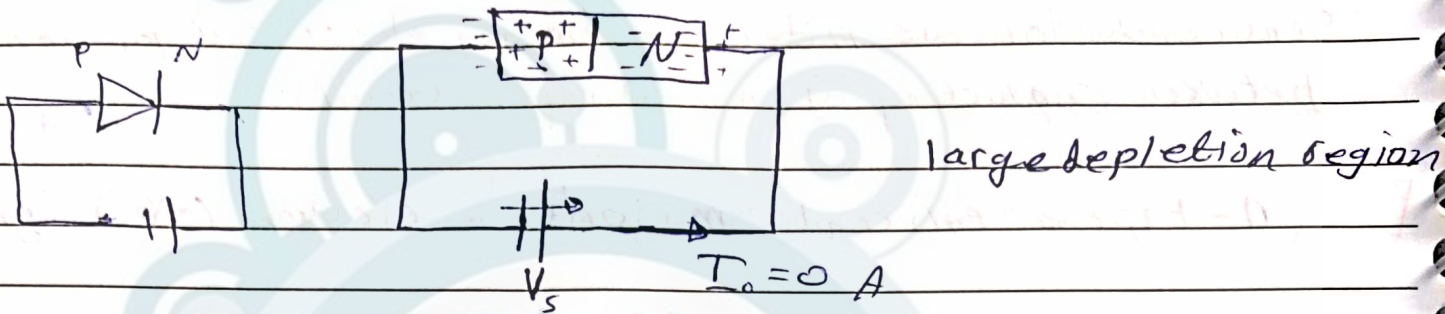


~~PN~~

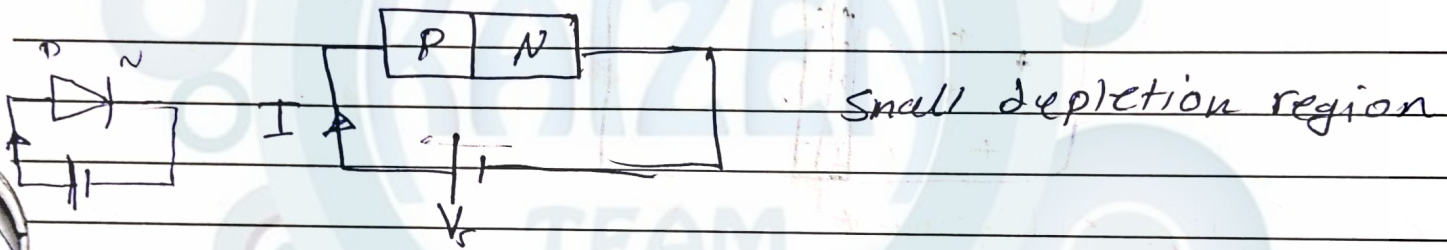
$\rightarrow$



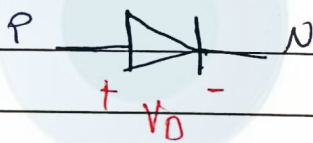
① Reverse Bias



② Forward Bias



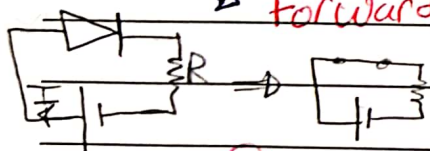
\* ideal diode :-  $V_D = V_p - V_n = 0$



$V_p > V_n \rightarrow$  Forward bias  
 $V_n > V_p \rightarrow$  Reverse bias

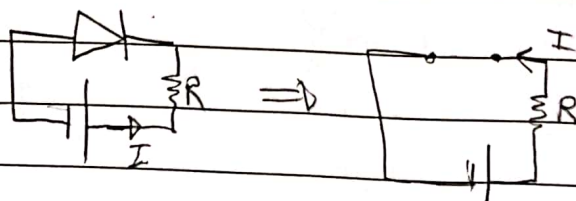
①

Forward Bias: diode is replaced by short circuit



Si  $\rightarrow$  0.7 V  
 Ge  $\rightarrow$  0.2 V

② Reverse Bias: diode is replaced by open circuit



# \* practical Diode:-

① Forward Biase: Diode is replaced by supply with value

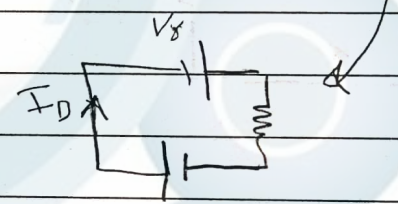
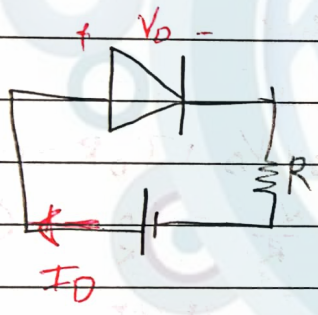
- of =  $V_s$ 
  - (0.6 - 0.7) si
  - (0.2 - 0.3) Ge

② Reverse Biase: open circuit

Forward: ① Forward off if  $V_D < V_s$  ( $i_D = 0$ )

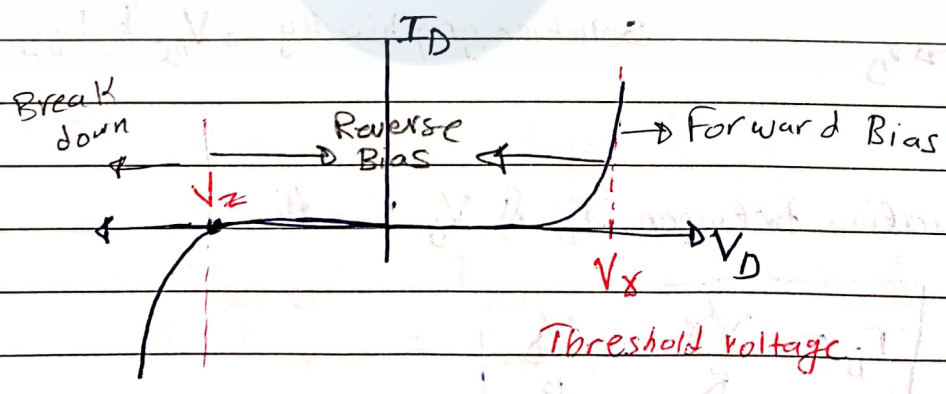
② Forward on if  $V_D > V_s$

$$I_D = (I_0 (e^{qV_D/kT} - 1))$$



$I_0 =$  saturation current ( $\mu A$ )

## I-V characteristic For diode

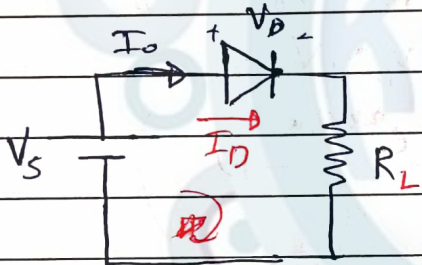




\* steps to solve to know if Diode is on :-

- ① replace diode by open circuit.
- ② Find  $V_D$  on diode
- ③ IF  $V_D > V_s$  = diode is on  
= replace it by voltage source have value of  $V_s$
- ④ IF  $V_D < V_s$  = diode is off  
= replace it by open circuit. ( $I=0$ )

\* load lines -

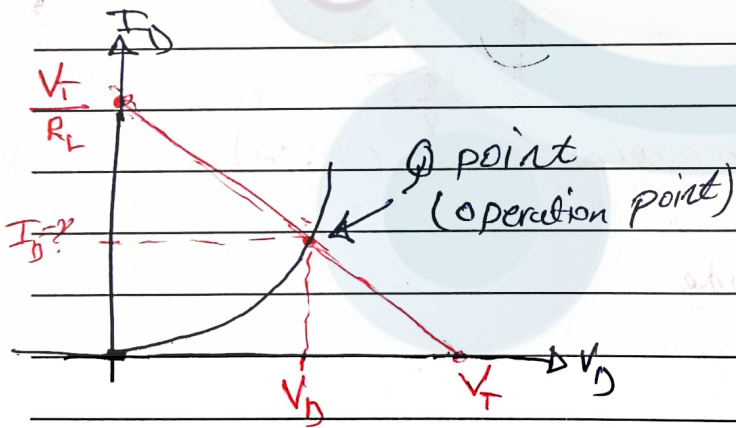


$I_D, V_D \Rightarrow$  unknowns.

using KVL  $\Rightarrow -V_s + V_D + I_D R = 0$

$$I_D = \frac{V_s}{R} - \frac{V_D}{R} \quad \text{--- (1)}$$

$$I_D = I_0 (e^{qV_D/kT} - 1) \quad \text{--- (2)}$$



graphs.  $\Rightarrow$   $V_{DQ}$  &  $I_{DQ}$

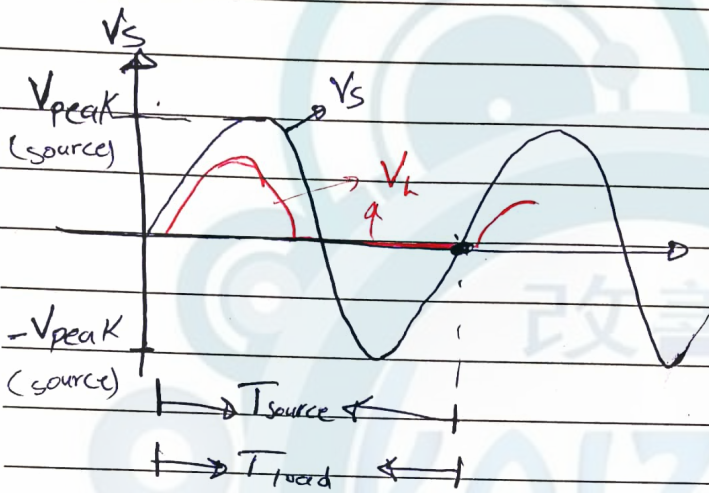
solution graphically  $\rightarrow V_{DQ}$  &  $I_{DQ}$

load line: equation between  $I_D$  &  $V_D$  For this

load line equ.

$$I_D = \frac{V_s}{R} - \frac{V_D}{R}$$

## \* half wave rectifier (HWR)



$$\Rightarrow T_{\text{source}} = T_{\text{load}}$$

$$P_{\text{source}} = P_{\text{load}}$$

$$\Rightarrow V_{L \text{ avg}} = \frac{1}{T} \int_0^T V_L(t) dt$$

$$V_{L \text{ avg}} = \frac{V_{L \text{ peak}}}{\pi}$$

$$\Rightarrow I_{L \text{ avg}} = \frac{V_{L \text{ avg}}}{R}$$

$$\Rightarrow I_{L \text{ peak}} = \frac{V_{L \text{ peak}}}{R}$$

$$V_{L \text{ peak}} = V_{S \text{ peak}} - V_d$$

DC & AC analysis \*

$$V_{\text{rms}} = \frac{V_{\text{peak}}}{\sqrt{2}}$$

$$V_{\text{peak}} = \sqrt{2} V_{\text{rms}}$$

## \* Full wave rectifier (FWR) using bridge

$$\Rightarrow T_{\text{source}} = 2 T_{\text{load}}$$

$$1/T_{\text{source}} = 1/2 T_{\text{load}}$$

$$\Rightarrow V_{L \text{ peak}} = V_{S \text{ peak}} - 2 V_d$$

$$\Rightarrow V_{L \text{ avg}} = \frac{2 V_{L \text{ peak}}}{\pi}$$

$$\Rightarrow P_{\text{source}} = P_{\text{load}}$$

$$\Rightarrow I_{L \text{ avg}} = \frac{V_{L \text{ avg}}}{R_L}$$