

# Thermal



الدكتور

جميل الافر



Thermal

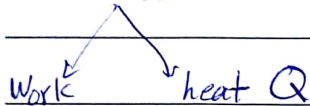
first part

1. thermo

Ch.1 Basic concepts.

Energy,  $E$ ,  $e = \frac{E}{m}$ ; kJ/kg,  $w = \frac{W}{m}$

$\rho = \frac{Q}{m}$



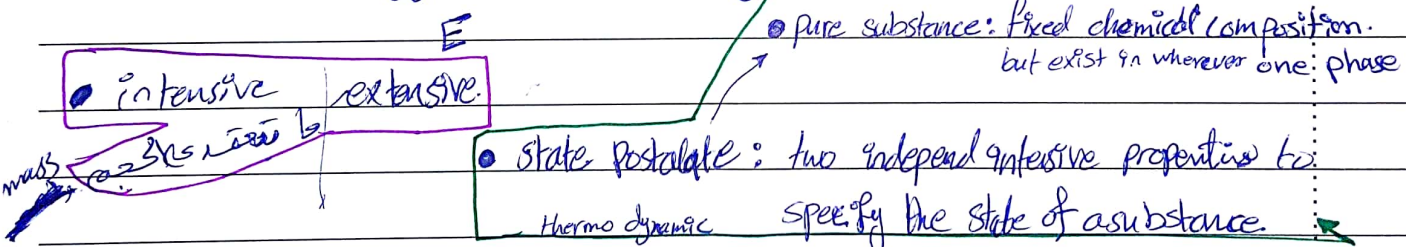
$\Delta E = Q_{net} - W_{net} = E_2 - E_1$ ;  $U$ : internal energy, kJ

K.E =  $\frac{1}{2} \vec{v}^2$  P.E =  $g \cdot Z$   
Potential

$e = u + k.e + p.e$

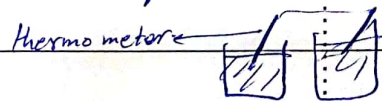
enthalpy,  $h = u + p v = u + \frac{p}{\rho}$ ;  $v = \frac{1}{\rho} = \frac{V}{m}$  specific volume ( $m^3/kg$ )  
 $\rho = \text{density } (kg/m^3)$

Flow work (energy) =  $P v$ ; entropy



0<sup>th</sup> (zeroth law) of T/D:

↳ If two bodies are in thermodynamic equilibrium with a third body, then they are in thermo. / D eq. with each other.



1<sup>st</sup> (first law) of T/D:

↳ Conservation of energy. Energy never created, no destroyed.

$\Delta E = E_2 - E_1 = Q - W$

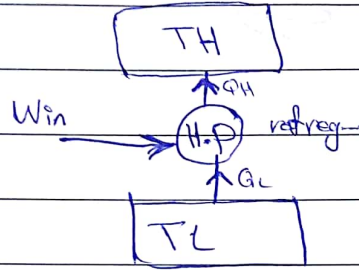
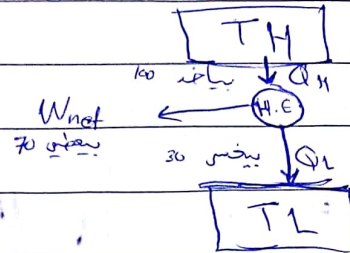
①



2<sup>nd</sup> (second law) of T/D.

process الالهة

I specifies that certain process occur in certain direction.



الدرجة المنخفضة  
 درجة الحرارة المنخفضة  
 الارتفاع

3<sup>rd</sup> (third law):

At zero kelvin, the entropy of pure crystalline is zero.

Second part:

$$2. H-T$$

Heat transfer.

\* Heat transfer

Conduction, convection, radiation.

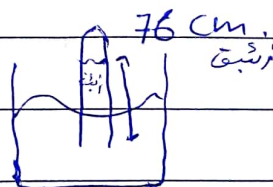
\* Fluid mechanics.

Static fluids, center of pressure.  $\rho = \frac{m}{V}$

Fluid in motion: continuity:  $m = \frac{dm}{dt} = \rho A v$

Bernoulli's eq-n.

parameter



Momentum =  $mv$

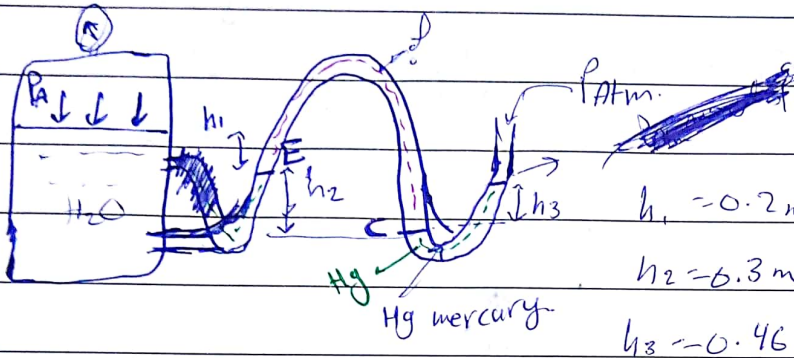
(2)

(2.55 - 2.66) five problems.

Mano meter

2-34 U-tube.

units!  
Calculations!



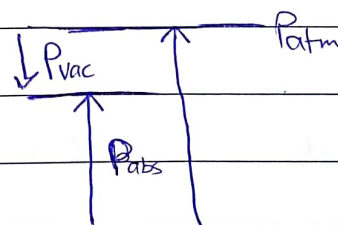
$h_1 = -0.2 \text{ m}$   
 $h_2 = -6.3 \text{ m}$   
 $h_3 = -0.46 \text{ m}$   
 $\rho_{Hg} = 13600 \text{ kg/m}^3$   
 $\rho_w = 1000 \text{ kg/m}^3$   
 $\rho_o = 850$

$P_a \text{ gage} = P_A - P_{atm}$

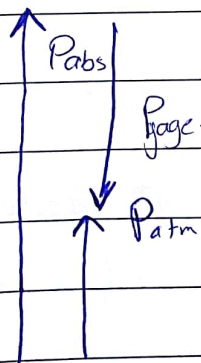
same level of same fluid

$P_{atm} + \rho_{Hg} g h_3 - \rho_w g h_2 - \rho_w g h_1 = P_A$

•  $P_{vac} = P_{atm} - P_{abs}$



•  $P_{gage} = P_{abs} - P_{atm}$



3



thermal

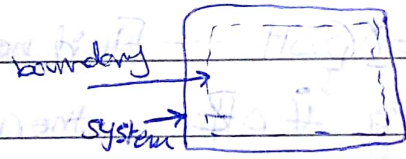
\*  $\Delta E = E_2 - E_1 = Q_{net} - W_{net}$   
 $= \Delta U + \Delta K.E + \Delta P.E$   
 For closed system.

but for open system (controlled volume)

أنظمة قياس درجة الحرارة ..

$x = \frac{5}{9}(x-32) + C = F$  at  $-40$   $\leftrightarrow$   $C = \frac{5}{9}(F-32)$

surrounding



gauge

vacuum.

$R = F + 460$

$K = C + 273.15$

$K = \frac{5}{9} R$

1 atm = 14.7 psi

independent properties

pressure & temperature

isobar saturation (phase change)

$W = \int_{x_1}^{x_2} P dx$

$P_g = \frac{F}{A} = \frac{mg}{A} = \frac{AZg}{A}$

$P_B = P_{atm}$

$P_B = P_{atm} + \rho Zg$

Work =  $W_b + W_{other}$

$W = \int F \cdot d = \int P \cdot A \cdot d = \int P \cdot \Delta V \rightarrow$  for closed system.  
 $= \int P \cdot V = P \cdot \Delta V$

W electrical  
 $I \cdot V \cdot \Delta t$

shaft

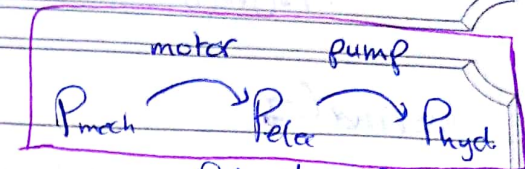
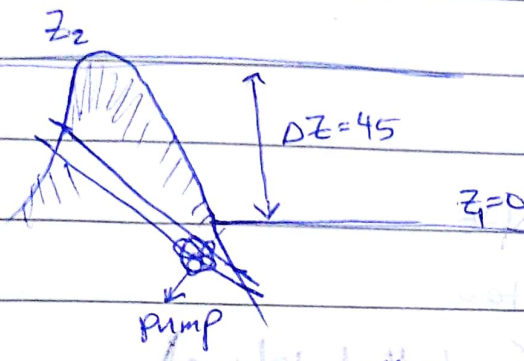
$= I \theta$   
 $= T \omega \Delta t$

$W_{spring} = \frac{1}{2} k(x_2^2 - x_1^2)$

• Spring =  $-kx$



3.66



$$\eta_{\text{motor}} = \frac{P_{\text{mech}}}{P_{\text{elec}}} = \frac{20}{25} = 80\%$$

$$\eta_{\text{pump}} = \frac{P_{\text{hyd}}}{P_{\text{elec}}} = \frac{13.24}{20} = 66\%$$

$P_{\text{mech}} = 20 \text{ kW}$      $P_{\text{elec}} = 25 \text{ kW}$      $\dot{V} = 0.3 \text{ m}^3/\text{s}$      $\rho = 1000 \text{ kg/m}^3$  ?

$$P_{\text{loss}} = P_{\text{mech}} - P_{\text{hyd}}$$

$$P_{\text{hyd}} = \rho \dot{V} \Delta H \quad \dots \text{Fluid mechanics.}$$

$$= \rho g \dot{V} \Delta z \quad \dots \text{thermal science}$$

$$= (1000)(9.8)(0.03)(45)$$

$$= 13243.5 \text{ W}$$

$$\frac{P_{\text{hyd}}}{P_{\text{elec}}} = \eta = 0.66 (0.8) = 52\%$$

P\_elec

18.6.19

اسم الطالب

رقم الطالب

Ch 2 Prozesse

التاريخ

evaporation, condensation, melting, freezing, sublimation

(i) isobaric process

constant pressure process  $P_2 = P_1$  (1-2)

(ii) isometric process

constant volume process  $V_2 = V_1$  (2-3)

(iii) isothermal process

constant temperature  $T_3 = T_1$

(iv) adiabatic process

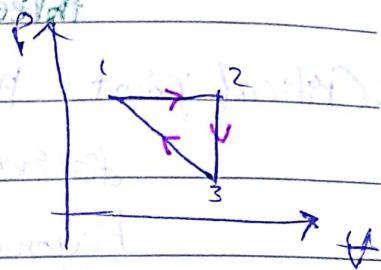
No heat transfer  $q = 0$  (isolated sys.)

(v) isentropic process

constant entropy process. (adiabatic + reversible)

(vi) isenthalpic process

constant enthalpy process



→ Continuum / simple compressible substance

fixed chemical composition without holes, uniform material & may exist in more phase.

$$S.G = \frac{\rho}{\rho_w}$$

6



Ch. 4 properties of pure substance.

- \* **Triple point**: The point at which the substance may exist in **three phases** (solid, liquid, gas) at equilibrium (i)
- \* **Critical point**: The point at which there is no further distinction between liquid & gaseous states. (ii)  
Beyond which the substance is called **supercritical fluid**. (iii)

19.6.19

CVI power

table A-11(c)

\*  $PV = mRT$  → for Ideal gas.

$C_p$ : specific heat at constant  $P$        $\Delta h = C_p \Delta T$

$C_v$ : specific heat at constant  $V$ .       $\Delta u = C_v \Delta T$

→  $k = \frac{C_p}{C_v}$  ,  $C_p - C_v = R$  #

T	P	linear interpolation.
$T_1$	$P_1$	$\frac{T_x - T_1}{T_2 - T_1} = \frac{P_x - P_1}{P_2 - P_1}$
$T_x$	$P_x$	
$T_2$	$P_2$	



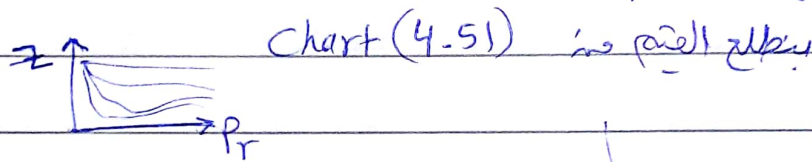
23.6.19

بسم الله

At  $P_{critical}$  (compressed table)

$$h = h_g @ T$$

Real Gas  $\rightarrow PV = ZRT$   $Z$ : compressibility factor



Equation of state  $PV = mRT$

$$X = \frac{m_g}{m_f + m_g} \quad \left( \frac{kg}{m^3} \right)$$

quality factor (4)

$$h = c_p T, \quad u = c_v T$$

section 4.8 X

$\rightarrow$  Prob (3<sup>rd</sup>)

29, 30, 32, 92, 60, 63, 101

$\rightarrow$  Compressed

$\Rightarrow$  super heated

الضغط أعلى

الحرارة أعلى

(8)



$$y = y_f + x y_{fg}$$

4-28 10kg of R-134a fill a 1.3589 m<sup>3</sup> rigid container at an initial temperature -40°C

(a) is heated until the R-134a exist as saturated vapor, find P<sub>2</sub> & T<sub>2</sub>?

(b) If heated continued, final pressure P<sub>3</sub> 200 kPa, find T<sub>f</sub>, Q & BW?

Sol :-

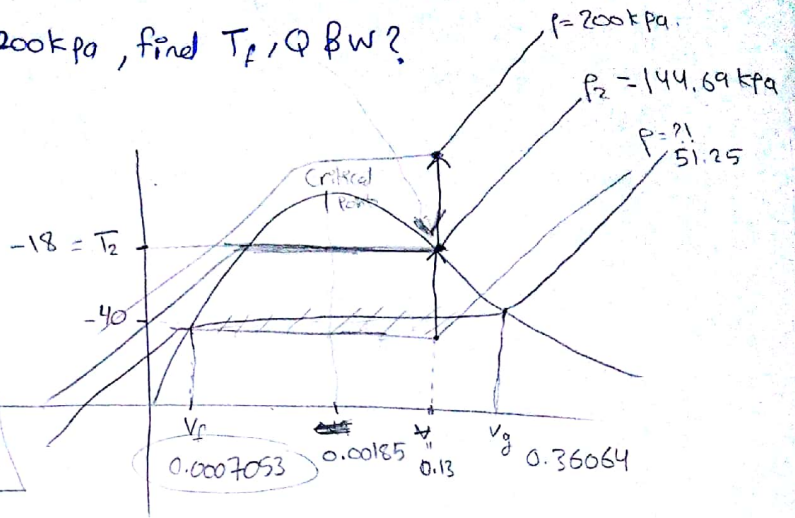
$$m = 10 \text{ kg}$$

$$V = 1.3589 \text{ m}^3$$

$$v = 0.13589 \text{ m}^3/\text{kg}$$

$$T_1 = -40^\circ\text{C}$$

We find v<sub>g</sub> & v<sub>f</sub> at -40 then compare it with our volume & critical volume



(a)

$$x = \frac{v_1 - v_f}{v_g - v_f}$$

$$x = \frac{0.13 - 0.000705}{0.36 - 0.000705} = 0.34$$

$$v_{crit} = \frac{0.19 \text{ m}^3/\text{mol}}{102.2 \text{ kg/mol}} = 0.00186$$

\*\* v<sub>1</sub> = v<sub>g</sub>

rigid body means constant volume

So v<sub>1</sub> = v<sub>2</sub> for all system (=)

$$U_1 = U_f + x U_{fg}$$

$$U_1 = -0.036 + 0.34(207.4)$$

(b) go to super heated table A-13

where P = 0.2 MPa & v = 0.13589 will find the T.

make interpolation

T	v	u
60	0.13206	279.38
T <sub>2</sub>	0.13589	x
70	0.13641	287.75

$$\frac{T_2 - 60}{70 - 60} = \frac{0.135 - 0.132}{0.136 - 0.132} \quad \left| \quad \frac{0.1358 - 0.132}{0.1364 - 0.1320} = \frac{x - 279.38}{287.7 - 279.3}$$

$$T_2 = 68.8 \quad U_2 = 286.73$$

$$Q = \dot{U} + U(m) = 10(U_2 - U_1) = 10(286.7 - 77.69) = 2090.4$$

$$\Delta E = Q - W = \Delta U + \Delta K + \Delta P = 0 \text{ closed system}$$



4-39

25.6.19

QWIPAW

water  $p_1 = 200 \text{ kPa}$ ,  $T_1 = 300^\circ\text{C}$  is contained in a piston-cylinder device fitted with stops, water is allowed to cool.

جیل اسیان

until the piston rests on stops (lower) where it exist as saturated steam.

const. V  
const. P  
const. V  
ثابت حجم  
ثابت دبی  
ثابت حجم

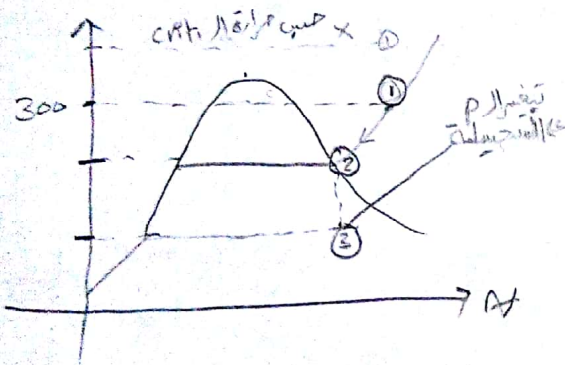
If cooling continues until final pressure ( $p_3$ ) reaches  $100 \text{ kPa}$ ,  $T_2, h, T_3, \Delta U, w, \dot{Q}??$

T-v & P-v diagrams!

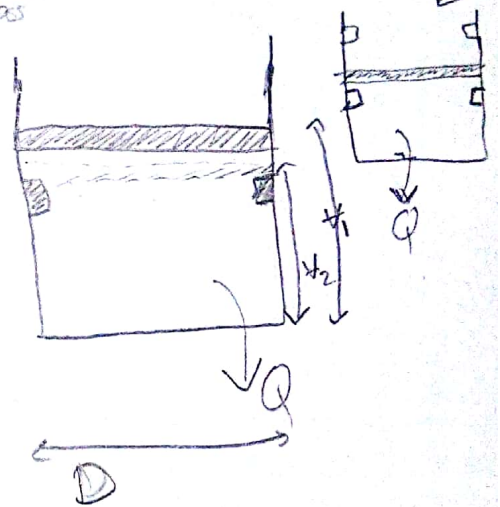
constant pressure then constant volume

$q = \frac{Q}{m}$   
Unit:  $\frac{\text{kJ}}{\text{kg}}$

SOL 37



جیل اسیان



State 1

super heated  $p_1 = 200 \text{ kPa}$ ,  $T_1 = 300^\circ\text{C}$

super heated  $v_1 = 1.31623 \text{ m}^3/\text{kg}$ ,  $u_1 = 2828.8 \text{ kJ/kg}$

State 2

(1-2) (cooling process) isobaric cooling process.

saturated vapor

$v_2 = 0.8857 \text{ m}^3/\text{kg}$ ,  $u_2 = u_g = 2529.1 \text{ kJ/kg}$

State 3

(2-3) (isometric cooling process); constant volume

saturated mix

$v_3 = v_2$

$T_3 = 99.61^\circ\text{C}$

$x = \frac{v_2 - v_f}{v_g - v_f}$

$x = \frac{0.88 - 0.00104}{0.88 - 0.00104} = 0.5236$

$u_3 = u_f + x u_{fg}$   
 $= 417.4 + 0.52(208)$   
 $= 1508.6 \text{ kJ/kg}$

$W_{1-3} = \int_1^3 P dv = \int_1^2 P dv + \int_2^3 P dv$   
 $= P_1(v_2 - v_1)$   
 $= 200(0.88 - 1.316)$   
 $= -86.09 \text{ kJ/kg}$   
(work done on system)

$= 0.5236$



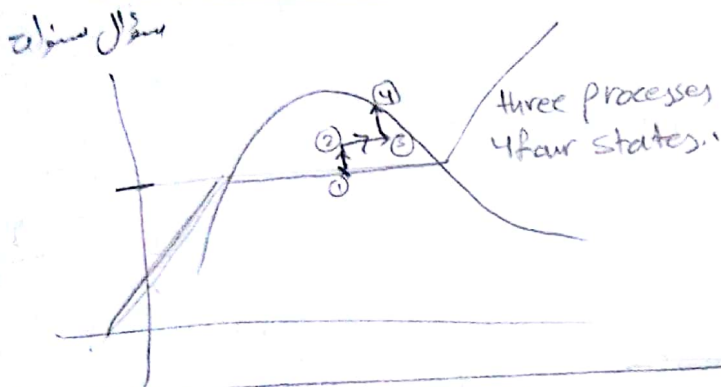
$$q_{1/3} - W_3 = \Delta E_3 = \Delta U + \Delta \bar{P} + \Delta \bar{K}$$

$$q_{1/3} = -86.09 + (158.6 - 2807.2)$$

$$= -1386. \text{ kJ/kg}$$

heat transfer from system. #

المنوال



iso thermal. ▽

Ch.5 Energy Analysis of closed system.

$$\Rightarrow \Delta E = Q - W ; W = W_b + W_{other}$$

$$W_b \rightarrow \text{(i) isometric } W_{12} = \int P dv = 0$$

and these (ii) isobaric  $P_2 = P_1 \rightarrow W_{12} = \int P dv = P_1 (V_2 - V_1)$

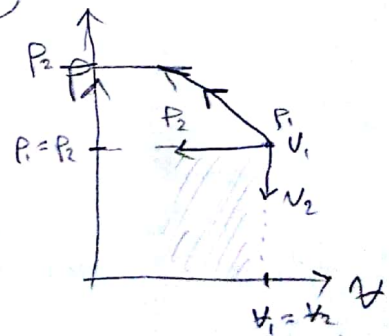
For Ideal gas.

(iii) isothermal  $T_2 = T_1$   $P_1 V_1 = P_2 V_2 = RT_1 = C$

$$P = \frac{C}{V} \rightarrow W_{12} = \int_{V_1}^{V_2} \frac{C}{V} dV$$

$$= C \ln V \Big|_{V_1}^{V_2}$$

$$= P_1 V_1 \ln \frac{V_2}{V_1} = R_1 T_1 \ln \frac{P_1}{P_2} \dots (5-10)$$



||

(2)

→

26-6-19

Q11 part

Just for Ideal gases

(iii) isobaric ;  $T_1 = T_2$  ;  $P_1 V_1 = P_2 V_2 = C = RT$

$$W_2 = \int_{V_1}^{V_2} \frac{C}{V} dV = PV \ln \frac{V_2}{V_1} = RT_1 \ln \frac{P_1}{P_2}$$

(iv) adiabatic & reversible (isentropic)  $S_1 = S_2, \delta Q = 0$

$PV = RT$  ;  $PV^\gamma = C = P_1 V_1^\gamma = P_2 V_2^\gamma$

$P = \frac{C}{V^\gamma}$

$$W_2 = C \int_{V_1}^{V_2} \frac{-\gamma}{V^{\gamma+1}} dV = \frac{C}{1-\gamma} \left[ P_2 V_2^{1-\gamma} - P_1 V_1^{1-\gamma} \right]$$

$$= \frac{P_2 V_2 - P_1 V_1}{1-\gamma} = \frac{R(T_2 - T_1)}{1-\gamma}$$

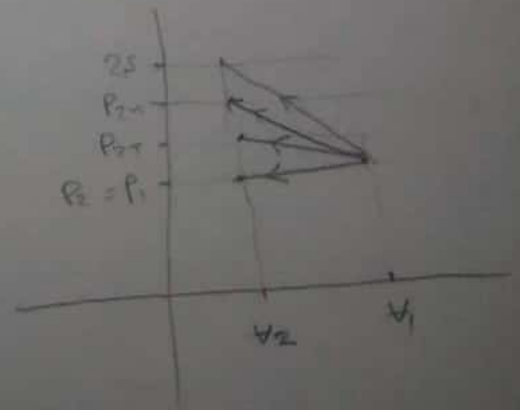
(v) Polytropic

$PV^n = \text{const.}$

$$W_2 = \frac{P_2 V_2 - P_1 V_1}{1-n} = \frac{R}{1-n} (T_2 - T_1)$$

more red. (st) process

$\gamma < n < \kappa$



S.32

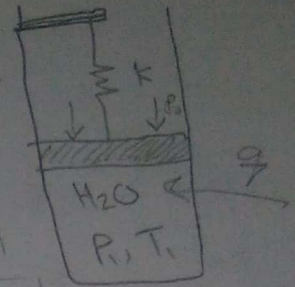
H<sub>2</sub>O, P<sub>1</sub> = 200 kPa, T<sub>1</sub> = 200°C, V = 0.4 m<sup>3</sup>

then P<sub>2</sub> = 250 kPa; V<sub>2</sub> = 0.6 m<sup>3</sup> → 0.608 m<sup>3</sup>

jumlah air 300 kPa

total air  
specific = 0.6

air di bagian



$$m = \frac{V_1}{v_1} = \frac{0.4 \text{ m}^3}{1.08049 \text{ m}^3/\text{kg}} = 0.3702 \text{ kg}$$

$$P_1 = P_0 + \frac{mg}{A}$$

air di bagian  
Piston.

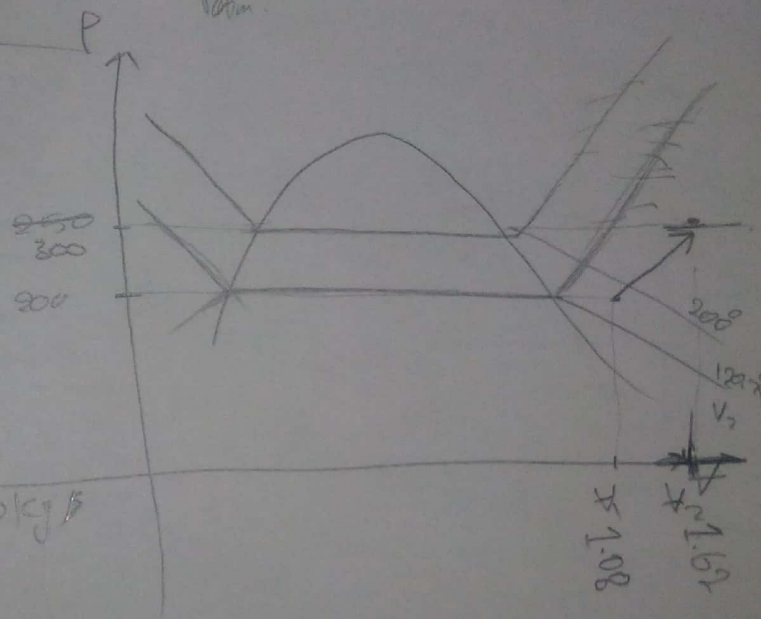
$$u_1 = 2654.6 \text{ kJ/kg}$$

$$v_2 = \frac{V_2}{m} = \frac{0.6}{0.3702} = 1.62075 \text{ m}^3/\text{kg}$$

$$W = W_b + W_{sp}$$

$$= \frac{P_1 + P_2}{2} (V_2 - V_1)$$

$$\left( \frac{200 + 300}{2} \right) (0.608 - 0.4) = 50 \text{ kJ}$$



$$T_2 \approx 800^\circ$$

$$u_2 = 3664.3 \text{ kJ/kg}$$

$$Q - W = \Delta u + \Delta k + \Delta p$$

$$Q - 50 = (0.37) (3664.3 - 2654)$$



30.6.19

QW/paw

Quiz

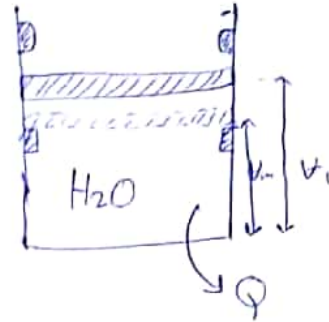
Prob (5.4) 5th edition (with doctored edit)

Piston-cylinder with two stops

$P_1 = 1000 \text{ kPa}$   $T_1 = 400^\circ \text{C}$  → Super heated steam

$v_{stop} = 0.4 v_1$   $P_f = 500 \text{ kPa}$

$m = 0.5 \text{ kg}$  |  $T_f?$   $Q?$   $W?$



Solution:

from A-6

$v_1 = 0.30661 \text{ m}^3/\text{kg}$

$u_1 = 2957.9 \text{ kJ/kg}$

$v_3 = v_{stop} = 0.4 v_1 \rightarrow 0.12264 \text{ m}^3/\text{kg} = v_2$

$P_2 = P_1 = 1000 \text{ kPa}$  ,  $T_1 = 400^\circ \text{C}$

$v_1 = v_{stop}$   $v_g$  at ~~1000~~ 1000 kPa in table A-11 we find  $T_2 = 179^\circ \text{C}$

$P_f = 500 \text{ kPa}$  ,  $v_{g2} = 0.193436 \text{ m}^3/\text{kg}$

$u_3 = ?$   $x_3 = \frac{v_3 - v_f}{v_{g3} - v_f} = \frac{0.12264 - 0.001093}{0.3748 - 0.001093}$

$x = 0.334$

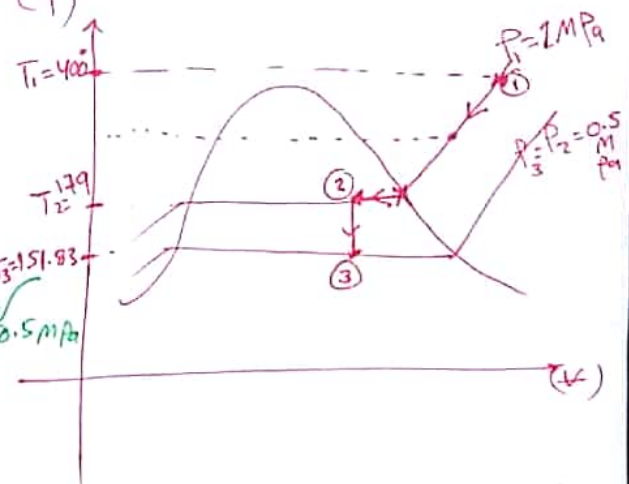
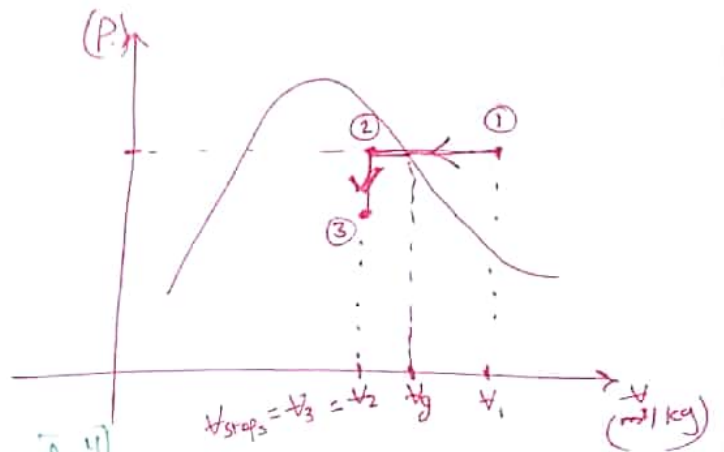
$u_3 = u_{3f} + x_3 u_{fg}$

$639.54 + 0.334 * 1921.2 = 1275.45 \text{ kJ/kg}$

$W = 1000(0.122644 - 0.30661)$

$W = -183.86 \text{ kJ/kg}$

$\Delta u = 1275.45$



$Q - W = m\Delta u + \Delta KE + \Delta PE$

#

1.7.19

all part

insulated  $q=0$

S.31

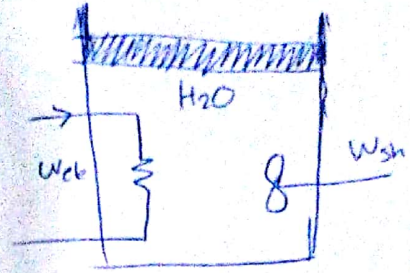
$$V_1 = 5L = 0.005 \text{ m}^3$$

$q=0$ , state ①: sat. liq.

$$P_1 = 175 \text{ kPa}, X_1 = 0$$

$$v_1 = v_f = 0.001057 \text{ m}^3/\text{kg}$$

$$u_1 = u_f = 486.82 \text{ kJ/kg}$$



State ②: Mixture

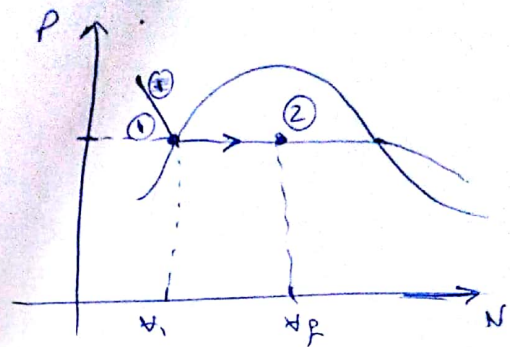
$$X_2 = 50 = 0.5$$

$$T_2 = T_1 = 116.04^\circ$$

$$P_2 = P_1 = 175 \text{ kPa}$$

$$v_2 = (1-X_2)v_f + X_2 v_g = 0.5023 \text{ m}^3/\text{kg}$$

$$u_2 = u_f + 0.5 u_{fg} = 1505.7 \text{ kJ/kg}$$



$$q - w = \Delta u + \Delta k + P \Delta v$$

$$\Delta u = -w$$

$$w = w_b + w_{other} = P(v_2 - v_1)$$

$$\Delta u = -[w_b + w_{sh} + w_{ele}]$$

$$1505.7 - 486.82 = [-87.71 - \frac{400}{m} + w_{ele}]$$

$$-1018.8 = 87.71 - \frac{400}{4.7} - \frac{(8)(V)(45)(60)}{(1000)(4.73)}$$

$$\frac{360 \times 60}{4730} = 1018.8 + 87.71 - \frac{400}{4.73}$$

$$V \approx 224 \text{ V}$$

$$w_b = P_1(v_2 - v_1)$$

$$= 175(0.5023 - 0.001)$$

$$= 87.7 \text{ kJ/kg}$$

$$w_{ele} = IV \Delta t \text{ [J]} \times 60 \text{ [s]}$$

$$= 1000 \text{ [kJ]} \times \text{mass [kg/kg]}$$

$$m = \frac{V_1}{v} = \frac{0.005}{0.001057} = 4.73 \text{ kg}$$

15



5-21

2.7.19

QW1 part

1 → 2 poly tropic  
 2 → 3 isobaric (isometric → isentropic)  
 3 → 1 isothermal

$$r = \frac{v_1}{v_2} = 8$$

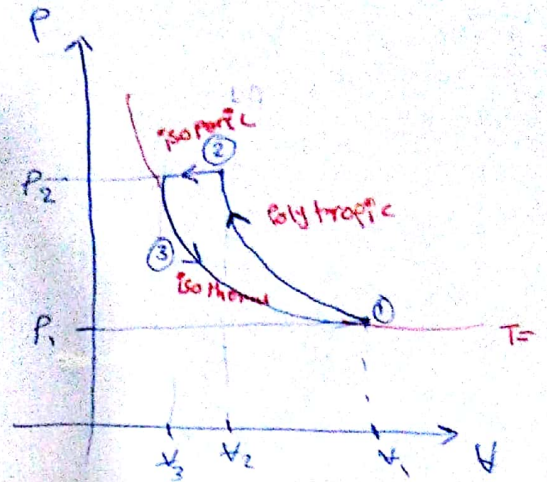
$$n = 1.2$$

$$P_1 = 100 \text{ kPa}$$

$$T_1 = 25^\circ$$

$$m = 1 \text{ kg } N_2(g)$$

$$P_2? T_2? P_3? T_3?$$



Solution

ideal gas

$$R = 0.2968 \text{ from A-1}$$

$$PV = mRT$$

$$(100 \text{ kPa})(v_1) = 0.2968(25 + 273)$$

$$v_1 = 0.8845 \text{ kg}$$

$$v_2 = \frac{v_1}{8} = 0.1106 \text{ kg}$$

$$P_2 v_2 = mRT_2$$

$$(1212.07)(0.1106) = (0.2968) T_2$$

$$T_2 = 451.67 \text{ K}$$

$$178.67^\circ$$

Warning! P in kPa

$$P_1 v_1^n = C \rightarrow (100)(0.884)^{1.2} = 86.305$$

$$C = P_2 v_2^n$$

$$86.305 = P_2 (0.1106)^{1.2}$$

$$P_2 = 1212.07 \text{ kPa}$$

$$P_3 = P_2 = 1212.07$$

$$P_3 = P_2 = 1212.07 \text{ kPa}$$

$$P_1 v_1 = P_3 v_3 \rightarrow (100)(0.884) = (1212.07)v_3$$

$$v_3 = 0.073 \text{ m}^3/\text{kg}$$

another way ↓

1 → 2

$$\frac{P_2}{P_1} = \left(\frac{v_1}{v_2}\right)^n = 8^{1.2} = 12.12 \rightarrow P_2 = 1212 \text{ kPa}$$

$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)\left(\frac{v_2}{v_1}\right) = \left(\frac{v_1}{v_2}\right)^n \left(\frac{v_2}{v_1}\right) = v_1^n \left(\frac{v_2}{v_1}\right)^{n-1} = r^{n-1}$$

$$T_2 = (298.15) \cdot (1.515)^{1.2} = 451.6 \text{ K} = 178^\circ$$



work

العمل  
الاجمالي

$$W = W_{12} + W_{23} + W_{31}$$

polytropic      isobaric      isothermal

$$= \frac{R(T_2 - T_1)}{1-n} + P_2(V_3 - V_2) + R T_3 \ln \frac{V_1}{V_3}$$

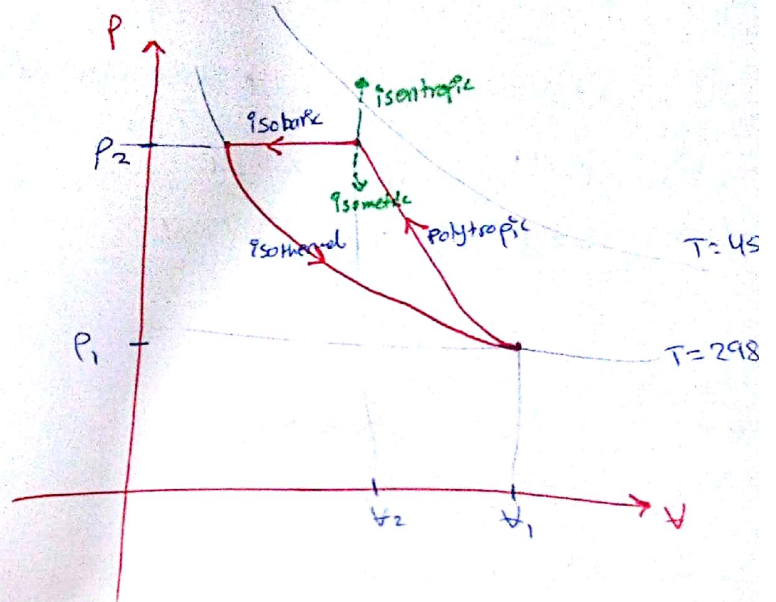
OR  $R(T_3 - T_2)$

$$q - W_1 = \Delta U + \Delta K + \Delta P$$

$$C_v(T_2 - T_1) = 0$$

ii) cycle  $\curvearrowright$

$$q = W$$



3.7.19

QW Paul

QW Paul

# closed system

$$\Delta E = \Delta U + \Delta K + \Delta P.E.$$

$$Q - w = \Delta U$$

Ideal gas

from doctor

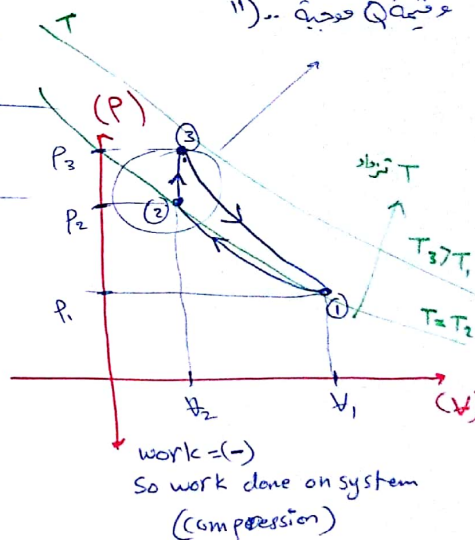
re-feed

Process	Q (kJ)	w (kJ)	ΔU (kJ)	Process type
1 → 2	-50	-50	0	$T_1 = T_2$ isothermal
2 → 3	+70	0	+70	isometric $V_2 = V_3$
3 → 1	0	+70	-70	adiabatic $Q = 0$
Cycle 1 → 2 → 3 → 1	+20 (70-50)	+20 (70-50)	0	

No heat transfer

T = 45

T = 298



DU سو سو اير  
(closed!) 0 = cycle سو

4.84 5th edition.

Ideal gas @  $P_1 V_1 = RT_1$

CO<sub>2</sub>(g)

$$P_1 V_1 = m R T_1 \rightarrow V_1 = \frac{2 \times 0.1889 \times 500}{3000}$$

$$V_1 = 0.063 \text{ m}^3/\text{s} = 63 \text{ liter/s}$$

$$V_2 = m R T_2 = \frac{2 \times 0.1889 (450)}{3000} = 56.7 \text{ lit/s}$$

Z (from chart) = 0.97

18

Per > 0.1  
Tcr > 2

Per = 7.39 ✓  
Tcr = 304.2 K ✓



9.7.19

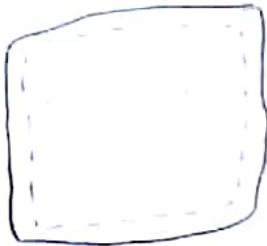
AWP

Ch. 6

First law: Energy analysis of control volumes / open systems

(i) Conservation of mass:  $m_1 + \sum m_{in} - \sum m_{ex} = m_2$

$\frac{dM}{dt} \Big|_{sys} = \sum \dot{m}_{in} - \sum \dot{m}_{ex}$



~~control volume~~

من  
انظمة  
متدفقة

$h = u + Pv$

$Pv = \frac{P}{\rho}$  (flow work)

$M_{system}$

(ii) Conservation of energy:  $\theta = h + \frac{V^2}{2} + gz$

$\Delta E = Q - W = m_2 \left( u_2 + \frac{V_2^2}{2} + gz_2 \right) - m_1 \left( u_1 + \frac{V_1^2}{2} + gz_1 \right) + \sum \dot{m}_{ex} \left( h_j + \frac{V_j^2}{2} + gz_j \right) - \sum \dot{m}_{in} \left( h_i + \frac{V_i^2}{2} + gz_i \right)$

(SSSF) Steady flow devices:-

(pump, turbine, expansion valve, ...)

$\sum \dot{m}_{in} = \sum \dot{m}_{ex} \dots (1)$

Single input - single output =  $\dot{m}_{in} = \dot{m}_e = \dot{m}$

$\Delta E = \dot{Q}_{net} - \dot{W}_{net} = \dot{m} (\Delta h + \Delta KE + \Delta PE)$

17 19

$$v = \sqrt{2gh}$$

ex.6-2

سرعة التي الطاقة من فرق  
 ارتفاع مع حجم التي الذي هو  
 كل من كل طول التي يتقل سرعتها



ex.6-3

لا بعلية البخار يستعمل  $v_p$

لا عند الفرج يستعمل  $v_g$  لا  $v_p$  gas.

هنا ينقسم  $h$  الى  $PE + KE$  عنان قبل الوحد

ينقسم في قسمين  $v_p$  و  $v_g$

$$m = \rho A \bar{V} = \frac{\rho A v_x}{v_g}$$

$\theta$ : total energy of flowing fluid.

$$\theta = h + \frac{v^2}{2000} + \frac{gz}{1000}$$



بِسْمِ اللَّهِ  
هَلْ لَكَ سُرْعَةٌ عِنْدَ اللَّهِ..!

10.7.19

ex. 6-3

Find @ flow energy in kw (b)  $Q = ?$

$$\textcircled{a} 173.9 \text{ kg/kg} * 2.37 \times 10^{-4} \text{ kg/s} = -0.041 \text{ kw}$$

$$\textcircled{b} Q - \dot{W} = \dot{m} \Delta \theta = \dot{m} (c_p \Delta T + \Delta P / \rho)$$

work in a  
rigid body

$$\dot{Q} = \dot{m} h_{fg}$$

$$\dot{q} = h_{fg} = 2226 \text{ kJ/kg}$$

ex. 6-5

الماء الساخن + الماء البارد

! عشان يبقى

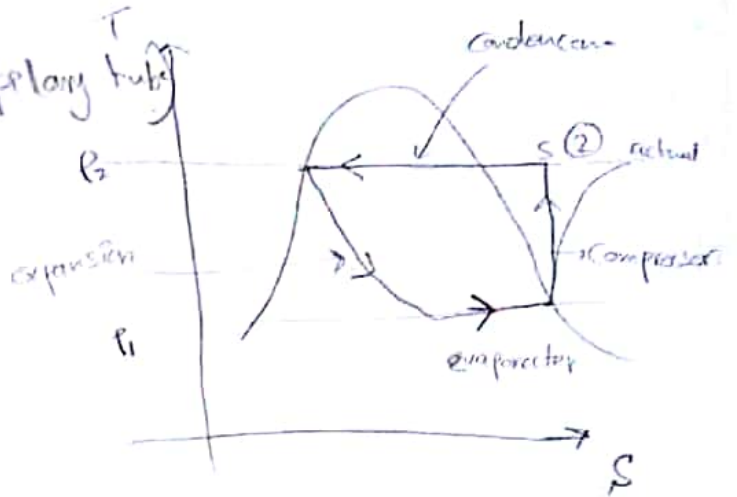
14.7.19

(W/raed)

Throttle or expansion valve (capillary tube)

Isenthalpic process,  $h_2 = h_1$

$P_2 < P_1$  &  $T_2 < T_1$

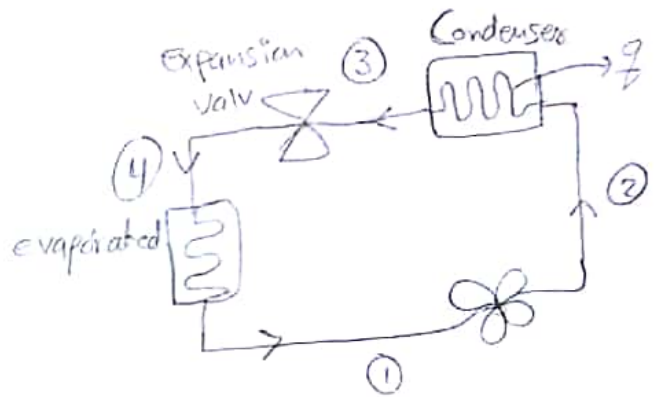


Jo + Jr  
ex. 6-8

$$\dot{q} - \dot{w} = \dot{A}h + \dot{A}k + \dot{A}p$$

$$\Delta h = 0$$

$$h_2 = h_1$$



refrigerator cycle.

Mixing chamber

=)  $\dot{m}_3 = \dot{m}_1 + \dot{m}_2$

ex. 6-9  
Jo + Jr

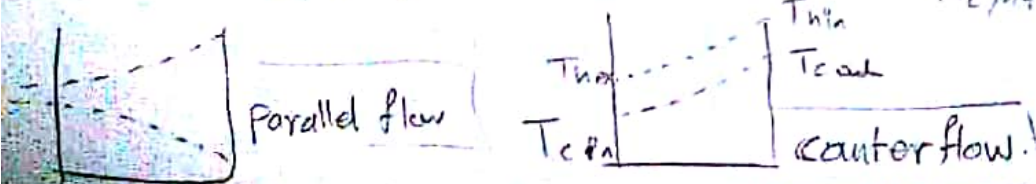
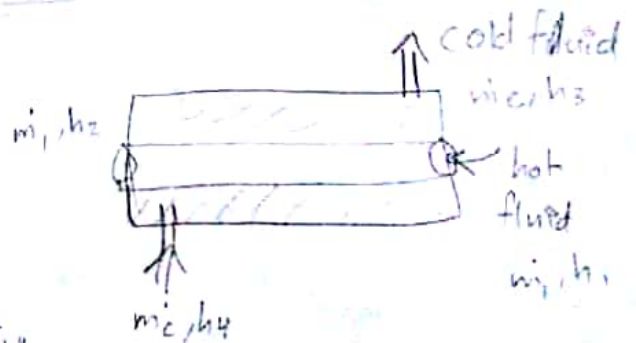
$$\dot{m}_3 = \dot{m}_1 + \dot{m}_2$$

$$\dot{m}_1 h_1 + \dot{m}_2 h_2 = (\dot{m}_1 + \dot{m}_2) h_3$$



Heat exchanger

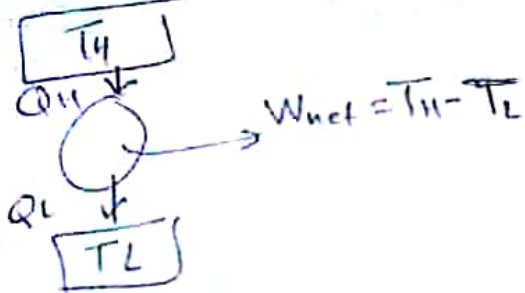
$$-\dot{m}_h (h_2 - h_1) = \dot{m}_c (h_4 - h_3)$$



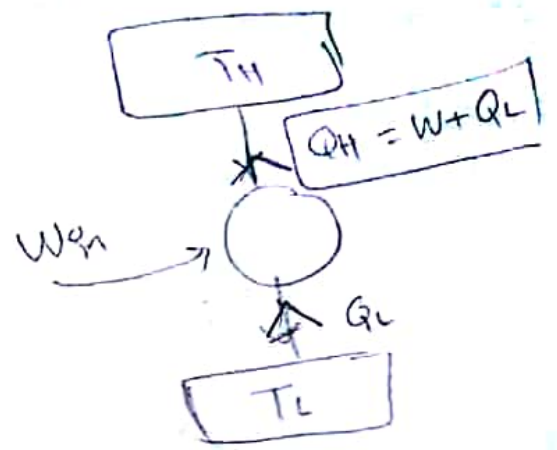




Ch. 7



Kelvin-Planck Statement



Heat-pump  
Clausius Statement

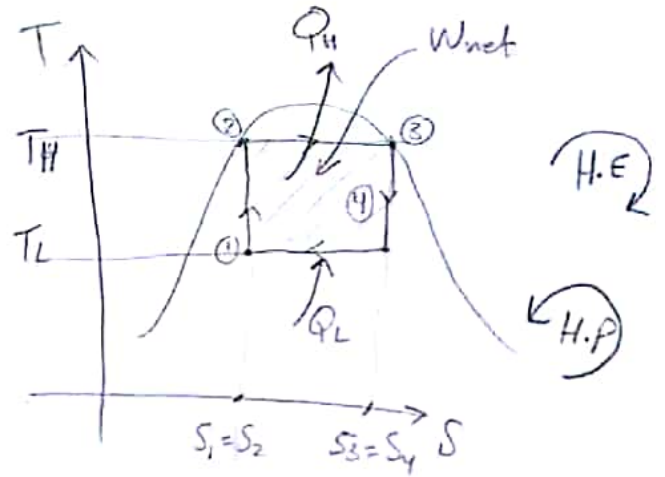
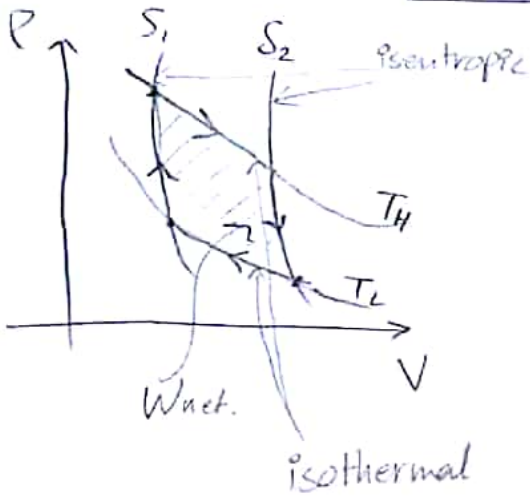


16.7.19

CW/pw

Carnot cycle.

for ideal gas



دایره کار  
کرنوت

$$\eta_{max} = \eta_{Carnot} = \frac{Q_H - Q_L}{Q_H} = 1 - \frac{Q_L}{Q_H} = 1 - \frac{T_L}{T_H} \quad (\text{reversible})$$

کارآمدترین چرخه  
تعمیراتی

17.7.19

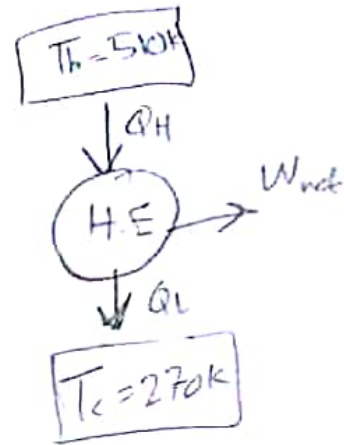
QVI Q.11

7.72

$$Q_H = W_{\text{net}} + Q_L$$

$$= 4.1 + 15,000 \frac{\text{kJ}}{\text{hr}} \times \frac{1 \text{ hr}}{3600 \text{ s}}$$

$$= 4.1 + 4.167 = 8.267 \text{ kW}$$



$$\eta_{\text{max}} = 1 - \frac{T_C}{T_H} = 1 - \frac{270}{510} = 47.059\%$$

$$\eta_{\text{th}} = \frac{W}{Q_H} = \frac{4.1}{8.26} = 49.63\% \quad \underline{\text{Not valid}}$$

$$\eta_{\text{max}} = \eta_{\text{Carnot}} = \frac{W_{\text{net}}}{Q_H} = \frac{Q_H - Q_C}{Q_H} = 1 - \frac{Q_C}{Q_H} = 1 - \frac{T_C}{T_H}$$

$$\eta_{\text{th}} < \eta_{\text{max}}; \quad \eta_{\text{th}} = \frac{W_{\text{net}}}{Q_H}$$

7.114 problem.

$$W_{\text{net}} = (T_H - T_L)(S_{fg})_{\text{H}_2\text{O}}$$

$$S = (1.2 T_L - T_L)(0.22) \quad S_{fg} = T_L S_{fg} (0.22) (0.22)$$

$$T_L = \frac{5}{(0.044) S_{fg}}$$

350K

1

26

open sys

$$Q_2 - W_{12} = \dot{m} h_2 + \dot{Q}_L + \dot{Q}_H$$

$$\dot{Q}_H - \dot{W}_{12} = -\dot{m} h_2 = \frac{25}{0.22} = 113.6 \text{ kJ/kg}$$

$$\dot{Q}_H = \dot{m} h_2 = 5 \text{ kg/s} \times 22.7 \text{ kJ/kg} = 113.5 \text{ kW}$$

$$Q_{H1} = \text{COP}_{HP} = \frac{\dot{Q}_H}{W_{in}}$$



21.7.19

QW1 part

عولاد المسان

6.39 Steam (from tables)  $\dot{m}_s = \frac{20,000 \text{ kg}}{\text{hr}} = \frac{1 \text{ hr}}{3600 \text{ s}} = 5.56 \text{ kg/s}$

A-6  $P_1 = 7 \text{ MPa}, T_1 = 500^\circ$

$h_1 = 3411.4 \text{ kJ/kg}$

$x_1 = 0.048157 \text{ m}^3/\text{kg}$

$P_2 = 40 \text{ kPa}, x_2 = 1$

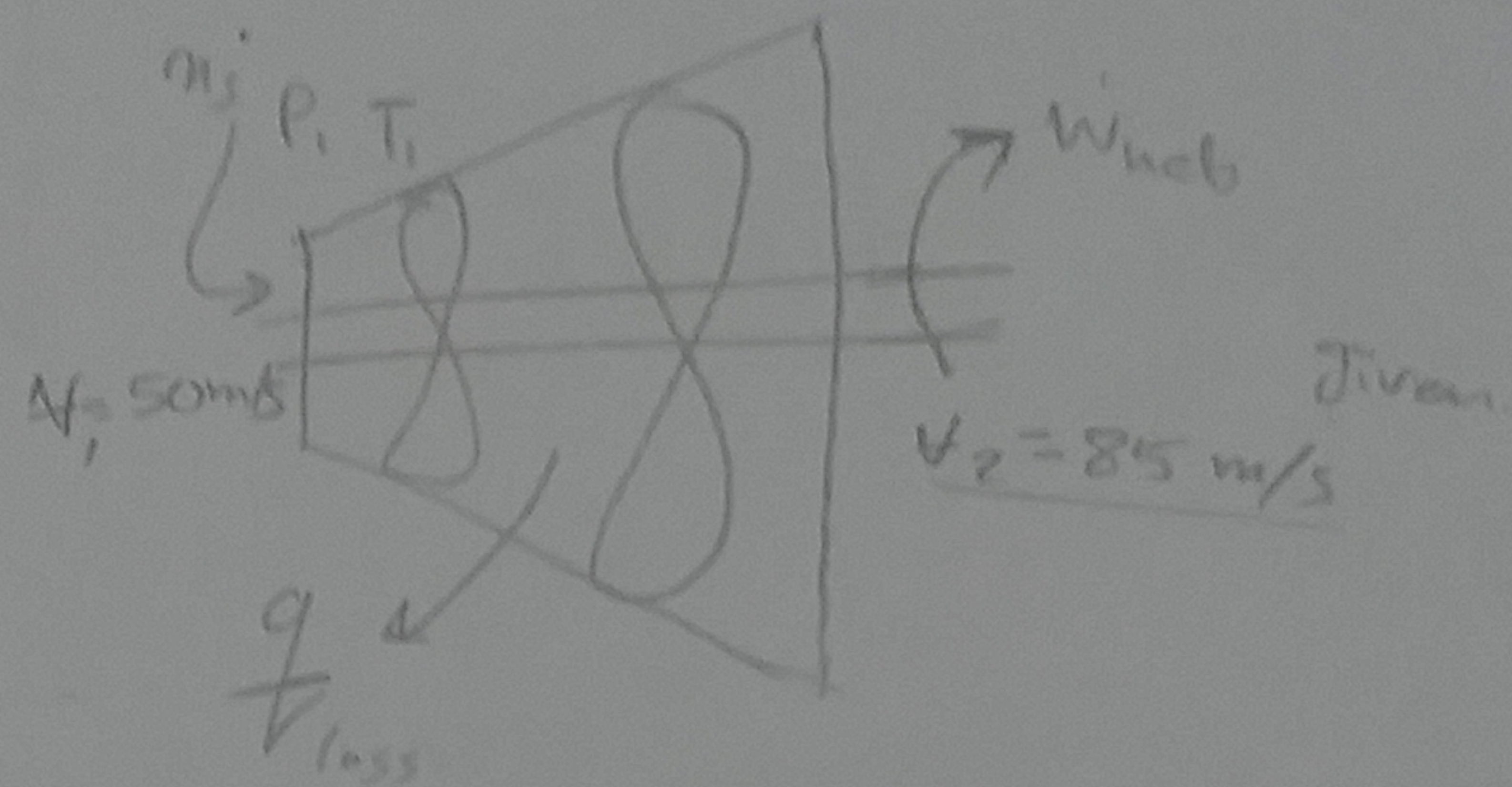
$h_2 = h_{g2} = 2636.1 \text{ kJ/kg}$

$x_2 = x_{g2} = 3.9933 \text{ m}^3/\text{kg}$

$\dot{Q} - \dot{W} = \dot{m}_s (\Delta h + \dot{q}_{loss} + \Delta p)$   
 $= (5.56) (2636.1 - 3411.4) + 400 \text{ V L/Lb}$

$Q = 4000 - 4309$

$= -309 \text{ kW}$



$x_2$   
 $x_2$   
 adiabatic  $q=0$   
 $w = \Delta h$

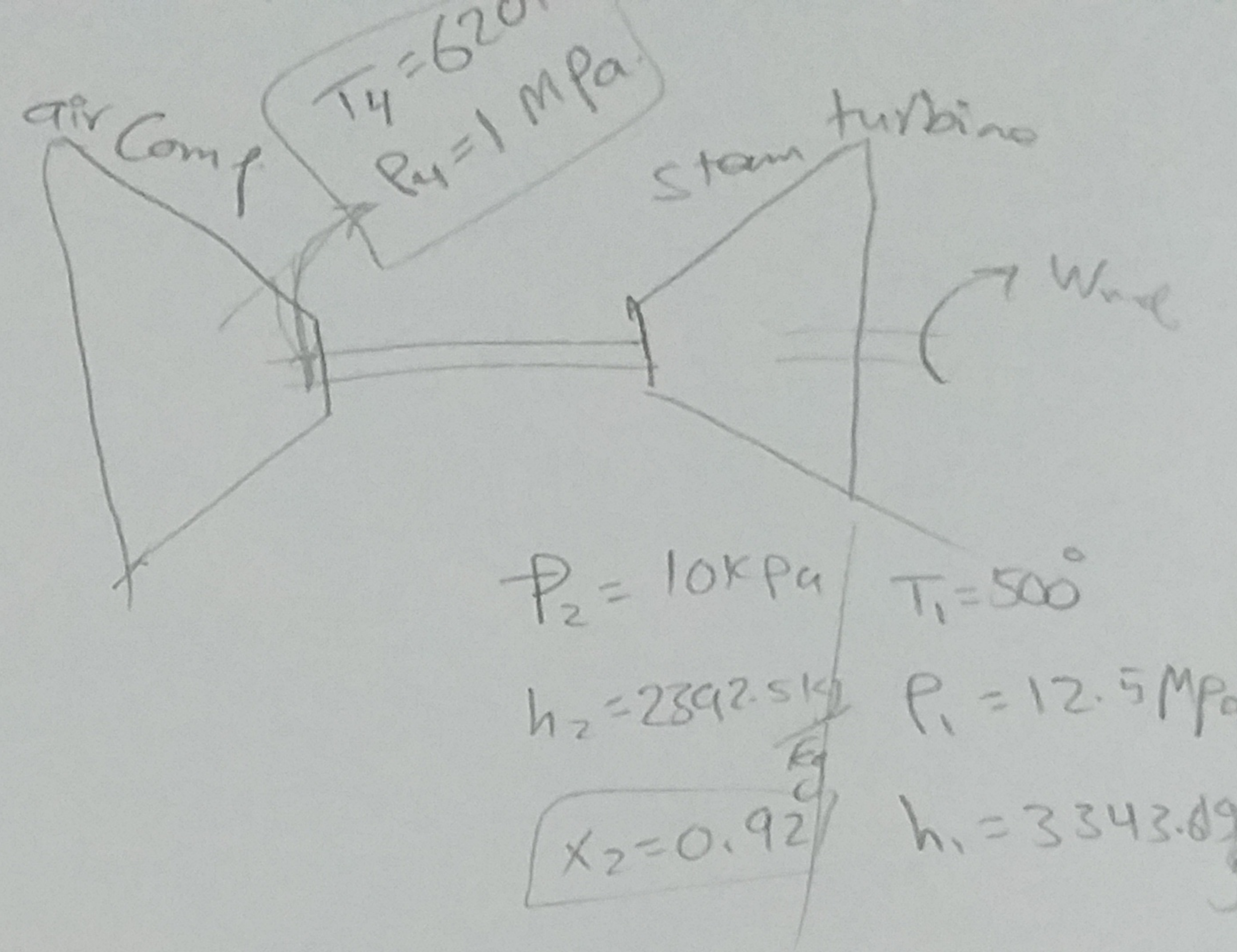
$V < 100$   
 velocity

$\dot{m} = \rho_1 A_1 \vec{V}_1 = \frac{\dot{m}}{A_1} \vec{V}_1 = \vec{A}_1 \vec{V}_1 = \vec{A}_1 V_1 = \frac{\dot{m}}{V_1} = \frac{5.56 \cdot 0.048}{50} = 48 \text{ cm}^2$

$A_2 = \frac{5.56 \cdot 3.9933}{85} = 2600 \text{ cm}^2$



6.145



$$W_{net} = \dot{m}_s W_s - \dot{m}_a W_a$$

$\dot{m}_s = 25 \text{ kg/s}$   
 $\dot{m}_a = 10 \text{ kg/s}$

$$\left(\frac{T_4}{T_3}\right) = \left(\frac{P_4}{P_3}\right)^{\frac{k-1}{k}}$$

Comp  $\Delta h$

$$\dot{Q} - \dot{W} = \dot{m}_a (C_p (T_4 - T_3))$$

$$-\dot{W} = 10.05 (620 - 295) = 3.25 \text{ kW}$$

Tur Air

$$\dot{Q} - \dot{W} = \dot{m}_s (h_2 - h_1) = 25 (2392.5 - 3343.6) = 23 \text{ MW}$$

$$W_{net} = 23 \text{ MW} - \frac{3.25 \text{ kW}}{CP \Delta h}$$

If  $\dot{W}_{net} = 0$   $\dot{m}_a (1.005) (620 - 295) = \dot{m}_s (h_2 - h_1)$

7.95 H.P.  $\dot{Q} = \frac{55000 \text{ kJ}}{3600} = 15.27 \text{ kW}$

$W_{in} = 4.8 \text{ kW}$

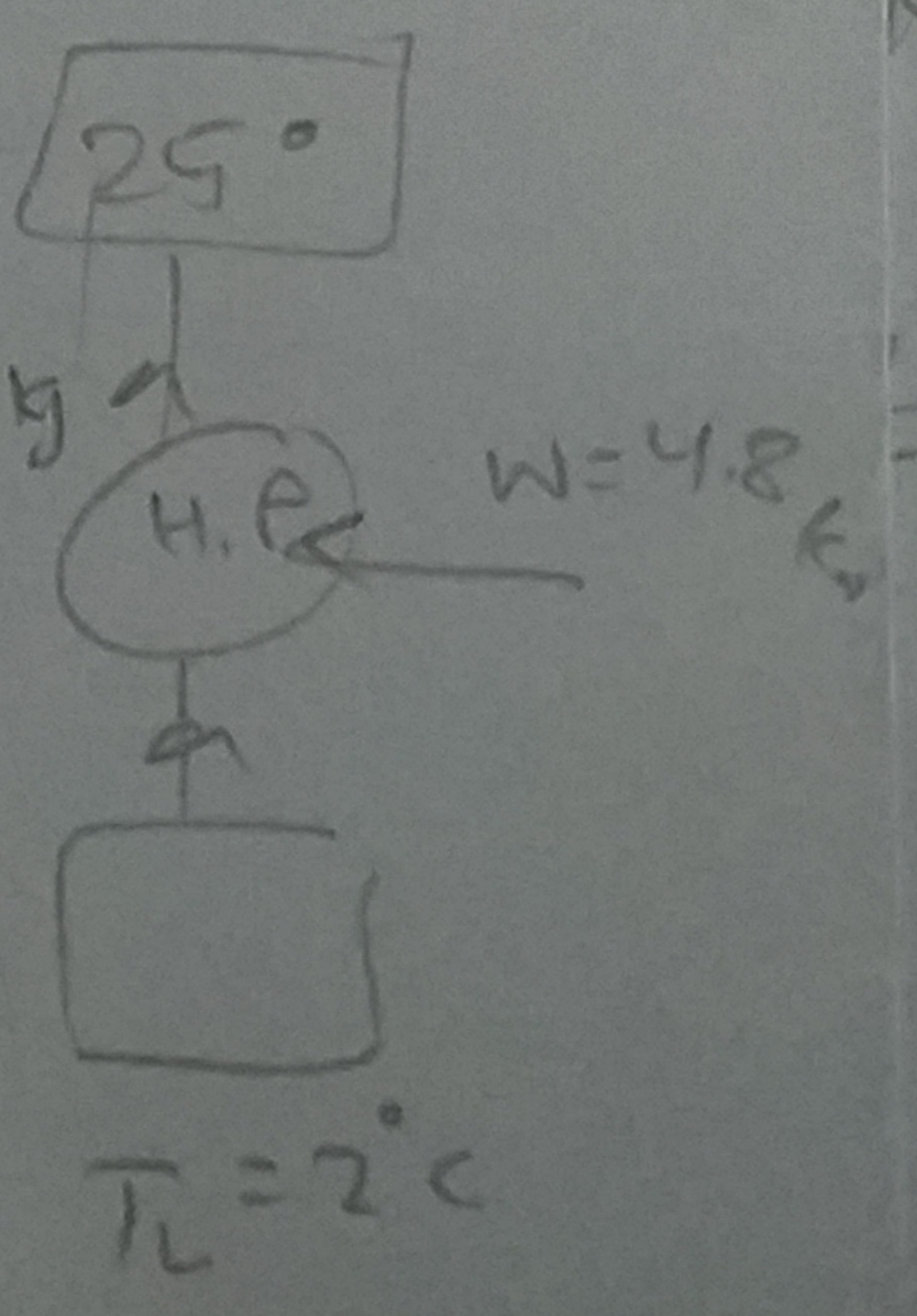
$Q = 1320000 \text{ kJ}$

$$\frac{Q_H}{W} = COP = \frac{1}{1 - \frac{T_L}{T_H}} = 12.9$$

$$\frac{1320000}{12.9} = W = 102325.5 \text{ kJ}$$

$W = Pt$

$$t = \frac{102325.5}{4.8 \times 3600} = 5.9 \text{ H}$$



$$\frac{4.8 \times 5.9 \times 11}{100} = 3.11 \text{ \$}$$

$$15.27 \times 24 \times 11 = 40.31 \text{ \$}$$

2

28



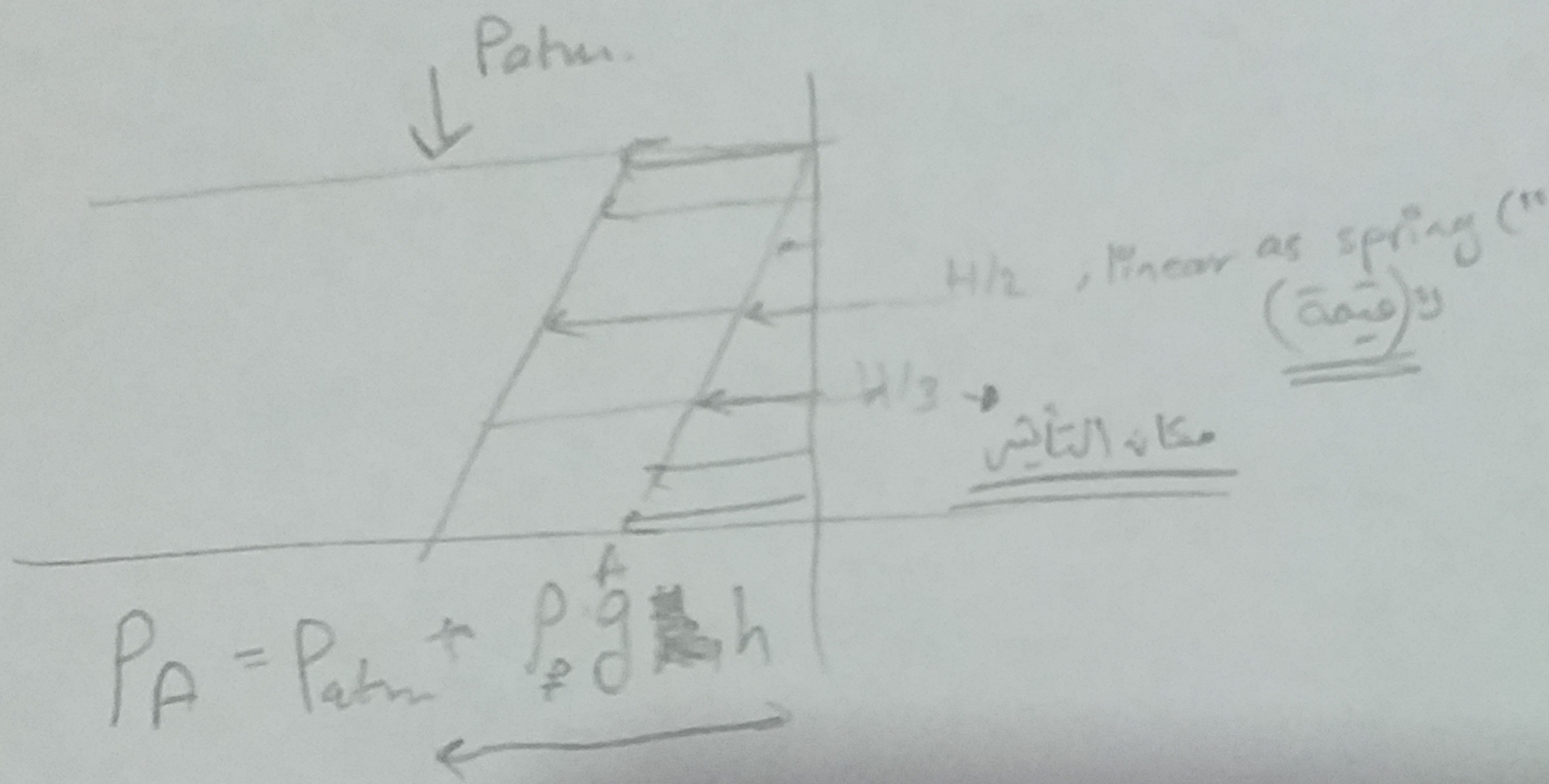
Fluids Mechanics / Statics, fluid flow.

↓  
Dams

Ch.2 } manometers  
Ch.3 }

Center of pressure, moment of force?

Fluids: liquids or gases, it can't resist shear stress



المتوسط  $\bar{P} = P_{atm} + \rho g H/2$

$F_p = \bar{P} A = [P_{atm} + \rho g H/2] A$

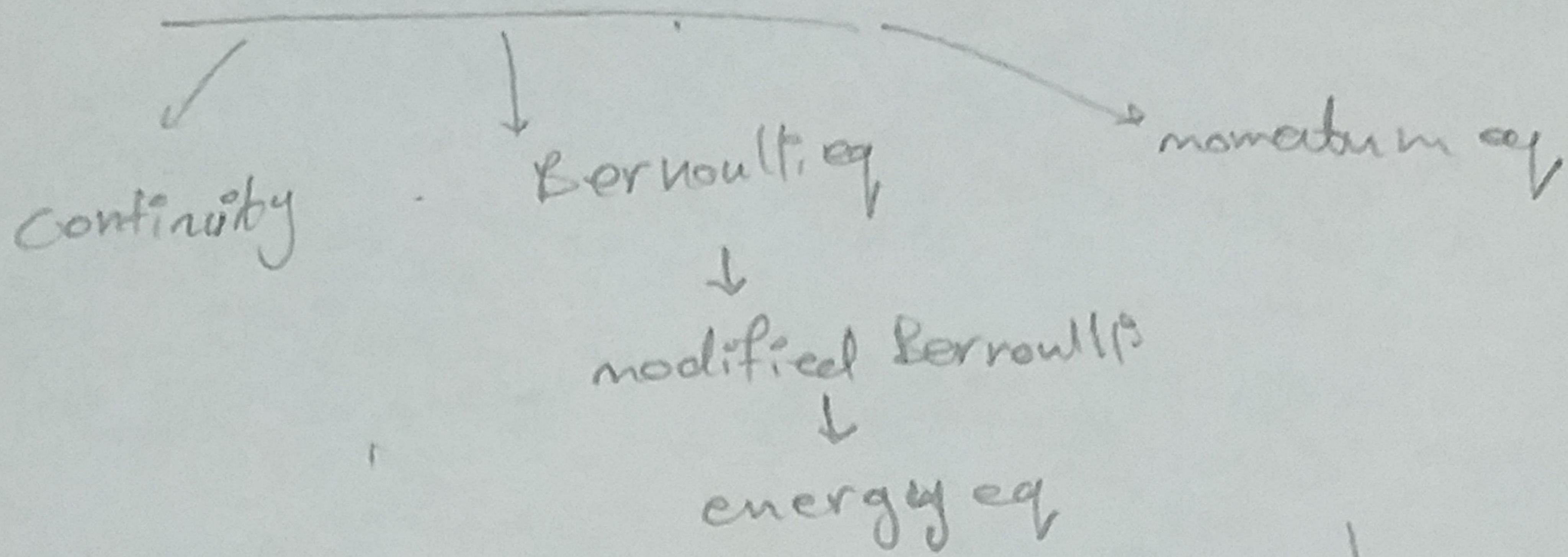
$A = L \times H \quad 1 \text{ m}^2$

h.c.p point of action is slightly lower than  $\bar{h}$  or  $\bar{y}$

$\sum M = 0 \quad \dots (1)$



# fluid flow



Read Ch 10

- ① internal & external flow
- ② Compressible & in
- ③ rotational & irro
- ④ Viscous & inviscid flow
- ⑤ Newtonian & Non-Newtonian fluid
- ⑥ laminar & turbulent flow.

math  $\vec{\omega} = 0$

$\vec{\nabla} \times \vec{V} = 0 \Rightarrow$  irrotational

$V = u\hat{i} + v\hat{j} + w\hat{k}$  m/s

$\vec{e}_r, \vec{e}_\theta$   
x axis

## Reynolds Experiment

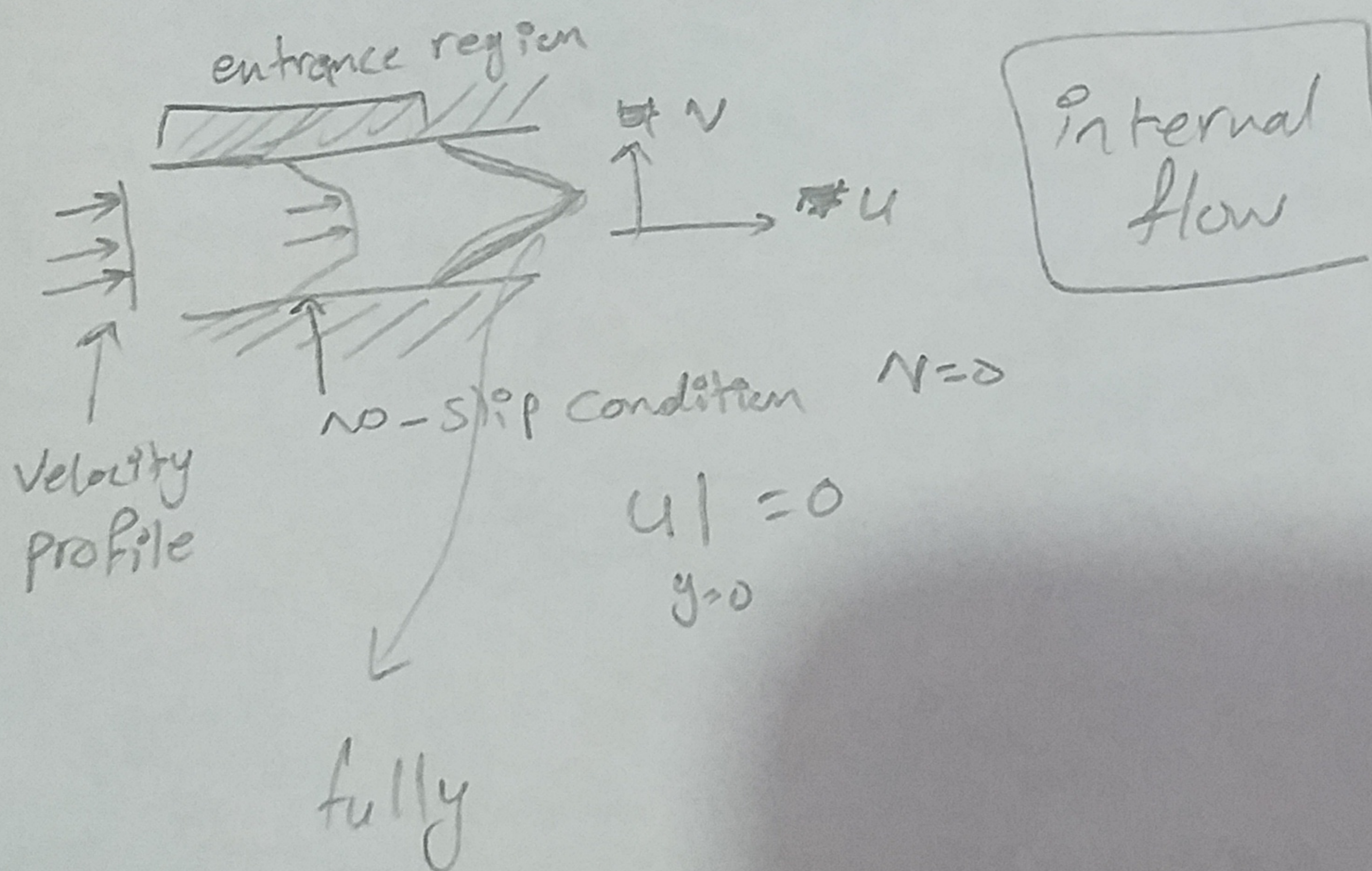
$Re < 2300$

laminar flow

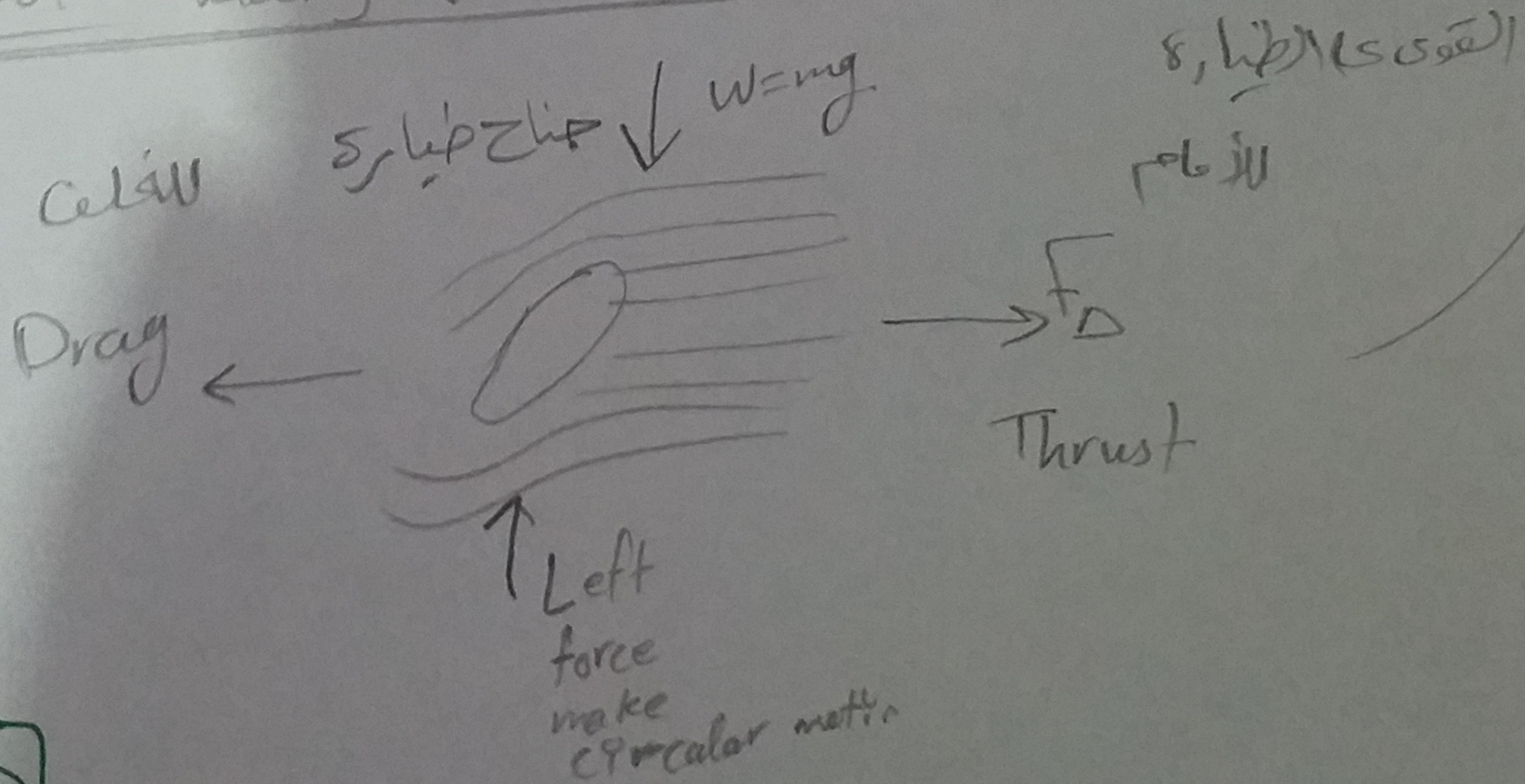
turbulent  $10^4$  أكبر

$f = (64/Re)$

$\epsilon/D$  turbulent roughness



turbulent velocity perpendicular to direction of motion





$$\delta = \frac{\mu}{\rho} \rightarrow \text{dynamic}$$

$$\text{kg/ms} = \text{N}\cdot\text{s/m}^2 = \frac{\text{kg}\cdot\text{m}}{\text{s}^2}\cdot\frac{\text{s}}{\text{m}^2}$$

kinematic  $\tau = \mu \frac{du}{dy} \rightarrow \text{Newtonian}$

$$\tau_{\text{max}} = \mu \left. \frac{du}{dy} \right|_{y=0}^{y=2r}$$

$\rho$  constant fluids  
liquids

$$h_{\text{loss}} = \frac{f L}{D} \frac{V^2}{2g} \quad \text{losses} \quad \rightarrow m.$$

moody diagram  
6 20 f 20 20

equation OR moody chart بظلمة الموائع



28.7.19

QWIPAW

Ch. 10 + 11 + 12

Static + elevation + dynamic = Bernoulli

piezometric head

$$\frac{P_1}{\rho g} + z_1 + \frac{V_1^2}{2g}$$

Bernoulli  $\bar{v}$   $\bar{v}$   $\bar{v}$

- incompressible
- irrotational
- inviscid
- steady

\* No slip  $\rightarrow$  means  $N=0$   
 (لا يوجد انزلاق)

Energy Equation.

$$h_{pump} + \frac{P_1}{\rho g} + \frac{V_1^2}{2g} = \frac{P_2}{\rho_2 g} + \frac{V_2^2}{2g} + z_2 + h_{loss} + h_{pump}$$

$$h_{loss} = h_{major} + h_{minor}$$

$$h_{loss} = \left( f \frac{L}{D} + \sum K \right) \frac{V^2}{2g}$$

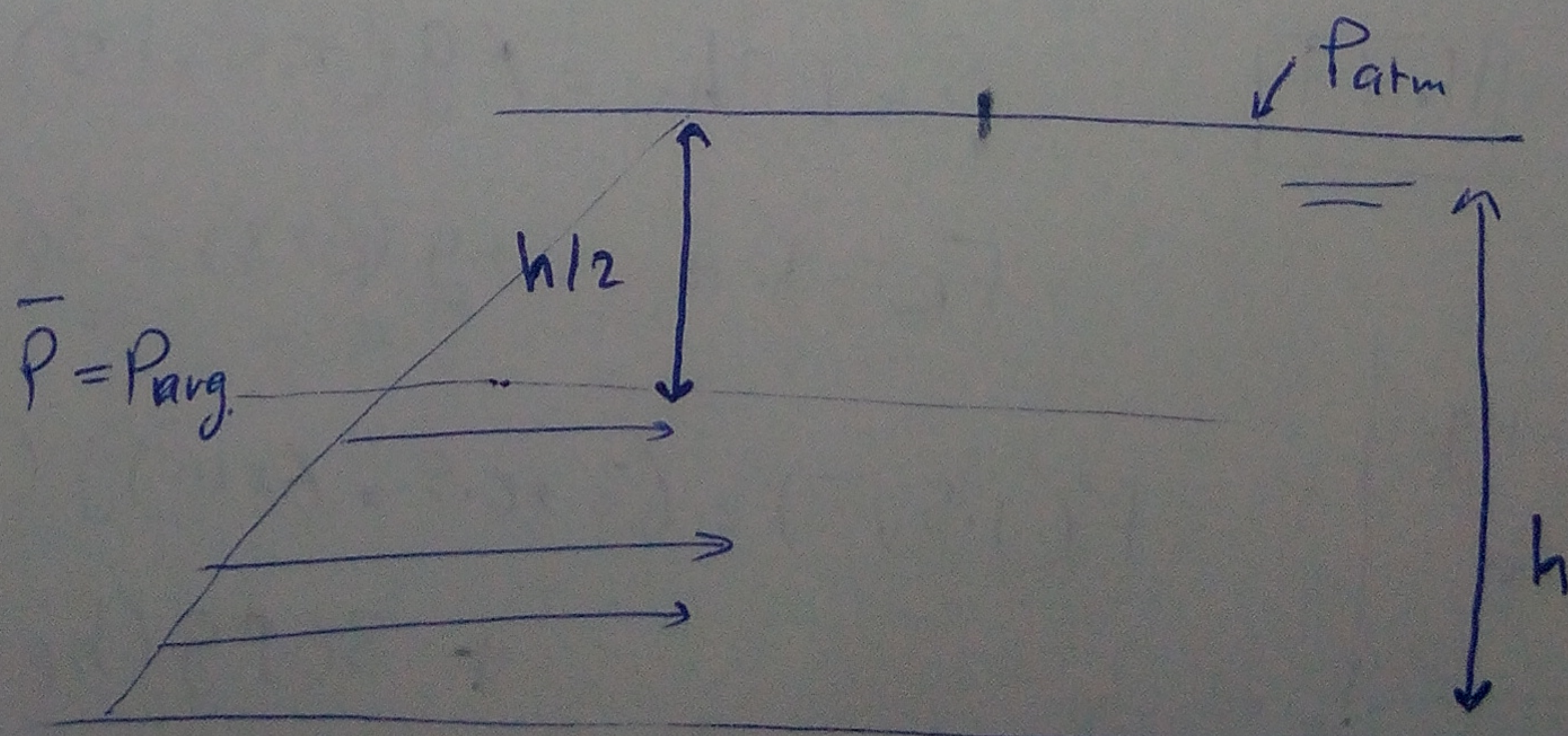
$$\bar{y} = y_c = h/2$$

$$h/2 = y_c \sin \theta$$

$h_{cp}$

$y_{cp}$

$$F_{cp} = \bar{P} A$$



$$P_A = P_{atm} + \rho g h$$



Figure 11.5

$$\vec{M} = \int_0^h \rho g y dA = \rho g b \int_0^h y^2 dy = (P_{atm} + \rho g h/2) A y_{cp}$$

$$\boxed{I = \bar{I} + Ad^2}$$
 Parallel axis theorem.

$$y_{c.p} = y_c + \frac{I_{xx,c}}{\left(y_c + \frac{P_0}{\rho g \sin \theta}\right) A}$$

$$y_{c.p} = y_p = y_c + \frac{I_{xx,c}}{y_c A} \quad \text{for } P_0 = 0 \quad (11.7b)$$

eq  $\Rightarrow$  11.10  $\rightarrow$  11.12  $\rho^0$

ex. 11.1  $y_{c.p} = s + \frac{b}{2} + \frac{b^2}{12\left(s + \frac{b}{2} + \frac{P_0}{\rho g \sin \theta}\right)}$

29.7.19

Ch. 11

قوى السائل

# Moment of Force

$\vec{M}_0 = \vec{r} \times \vec{F}$ , force time the perpendicular distance between the line of the force & the point at which the moment is calculated (Pivot point)

Problem 11.49

$$\bar{P} = \rho g h_c = \rho g (0.5 + 1.5) = 2\rho g$$

$$F_R = \bar{P} A = 2\rho g (6 \times 3) = 36\rho g$$

$b = 6m$   
 $m = 280 kg$   
AB gate

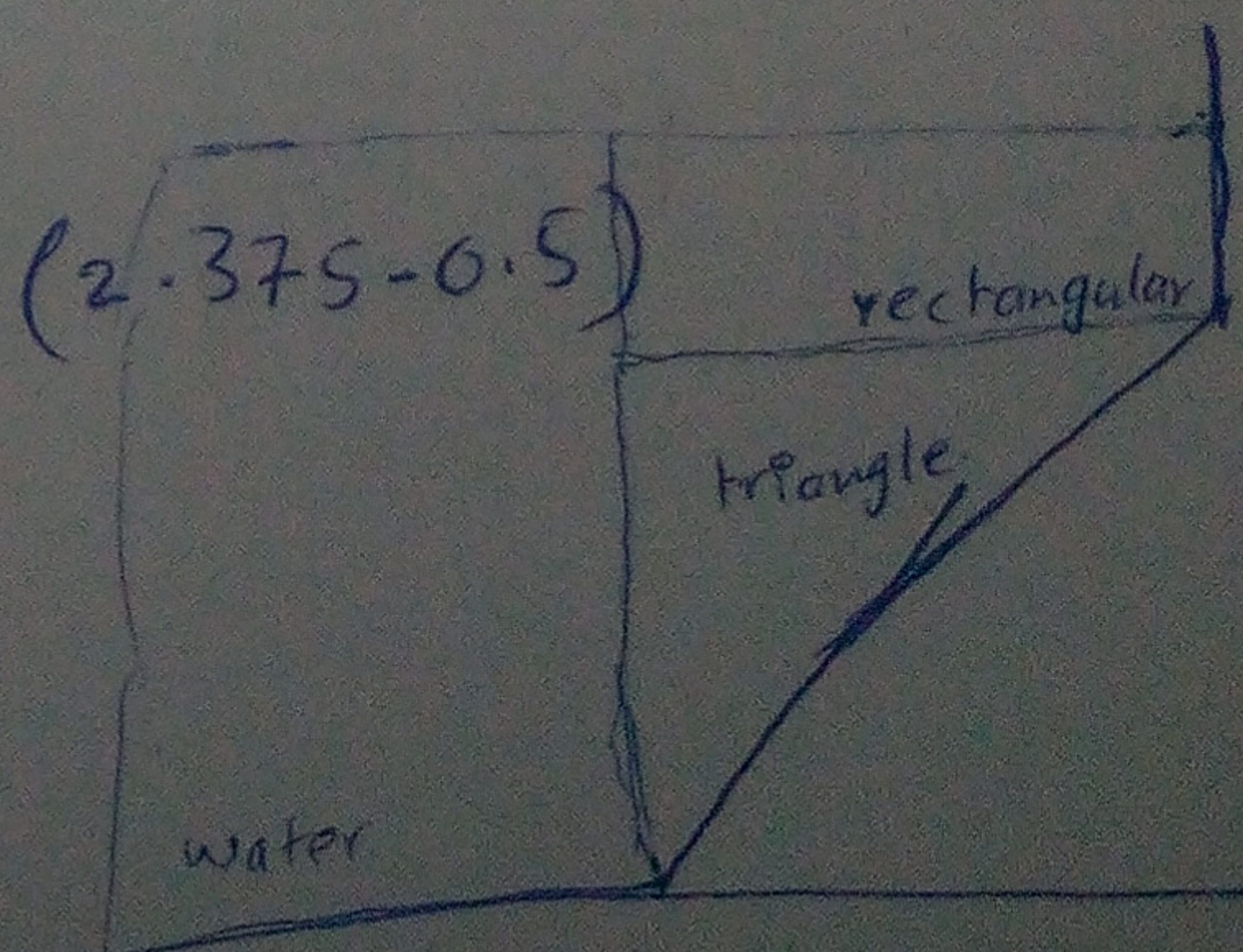
$$F(1.5\sqrt{2}) = (3 + 0.5 \times 6 \times 10^3)g(1.5) + (3 \times 1.5 \times 6) \times 10^3 \times g \times 2 + 36\rho g(h_p - 0.5)$$

$$h_p = h_{cp} = 0.5 + 1.5 + \frac{3^2}{12(0.5 + 1.5)}$$

$$1.5\sqrt{2} F = 13.5\rho g + 54\rho g + 36\rho g(2.375 - 0.5)$$

$$F = \frac{135\rho g}{1.5\sqrt{2}} = 624 kN$$

$h_p = 2.375 m$  عوض المسافة





30.7.19

نمایه عکس

All paid

Solve ex 11-8

Energy equation.

$$P_1 = P_2 = P_{atm}$$

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 + h_{pump} = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + h_{turb} + h_{loss}$$

$$z_1 = z_2 + h_{loss}$$

$$h_{loss} = \left( f \frac{L}{D} + \sum_{i=1}^5 K \right) \frac{V_{velocity}^2}{2g}$$

$N \neq V_1 \neq V_2$   
Velocity in pipe.

table A-15 to find  $f$  $f$  &  $V$ ?

$$\bar{V} = \frac{Q}{A} = \frac{0.006}{\pi (0.05)^2} = 3.05 \text{ m/s}$$

$$Re = \frac{\rho \bar{V} D}{\mu} = \frac{10^3 \times 3.05 \times 0.05}{1.307 \times 10^{-3}} \approx 117,000 \quad \text{So, turbulent.}$$

$$\frac{\epsilon_{rel}}{D} = \frac{\epsilon}{D} \quad (\text{from table 14-2}) = \frac{0.26 \text{ mm}}{50 \text{ mm}} = 0.0052$$

from moody chart  $f = 0.0315$ 

$$z = 4 + \underbrace{\left( 0.0315 \right) \left( \frac{89}{0.05} \right)}_{\text{major}} + \underbrace{\left( 0.5 + 2 \times 0.3 + 0.2 + 1.06 \right)}_{\text{minor}} \left( \frac{3.05^2}{2 \times 9.81} \right)$$

$$\boxed{z = 31.9 \text{ m}} \#$$



31.7.19

المسألة

Problem

14.26

تدفق السائل

laminar, Newtonian, fully developed

$$u(y) = U_0 \left(1 - \left(\frac{y}{h}\right)^2\right)$$

$$U_0 = u|_{y=0} = U_0$$

$$\dot{m} = \rho A \bar{V} = \rho A U_{av}$$

$$A U_{av} = \int 2 u(y) dA, \quad dA = 1 dy$$

$$U_{av} = \frac{2}{A} \int_0^h u(y) dy = \frac{2U_0}{2h} \int_0^h \left(1 - \left(\frac{y}{h}\right)^2\right) dy$$

$$= U_0 \left(y - \frac{y^3}{3h^2}\right) \Big|_0^h = \frac{U_0}{h} \left(h - \frac{h^3}{3h^2}\right) = \frac{2}{3} \frac{U_0 h}{h}$$

$$\tau(y) = \mu \frac{du}{dy} = \mu \left(-2 \frac{U_0 y}{h^2}\right)$$

$$u(y) = U_0 - \frac{U_0}{h^2} y^2$$

$$\frac{du}{dy} = 0 - \frac{2U_0}{h^2} y$$

$$\tau(y) = -2 \frac{U_0}{h^2} \mu y$$

$$A = 2h \times 1 = 2hm^2$$

4.8.19

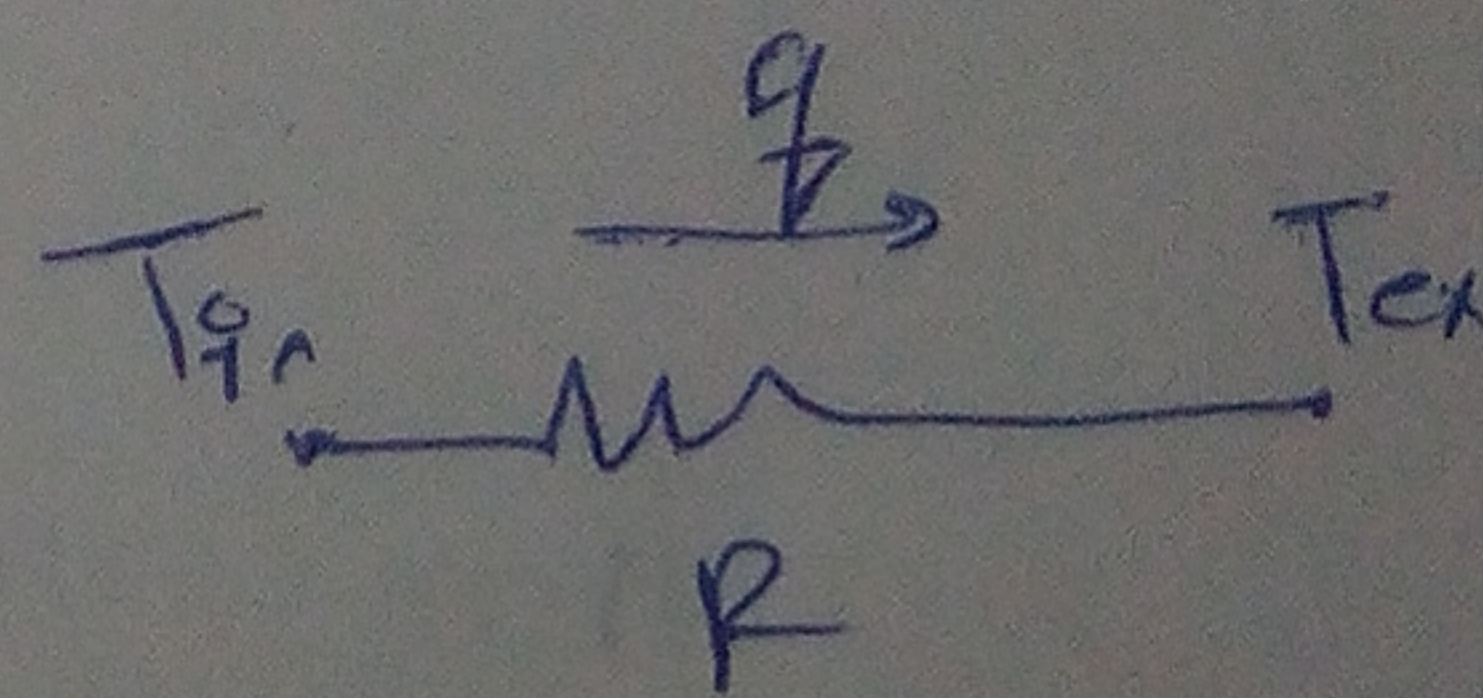
المسألة

Ch.16 Heat transfer

+17

① Conduction

$$q_{cond} = -KA_c \frac{dT}{dx} \approx -KA \frac{\Delta T}{\Delta x} = -KA \frac{\Delta T}{L}$$



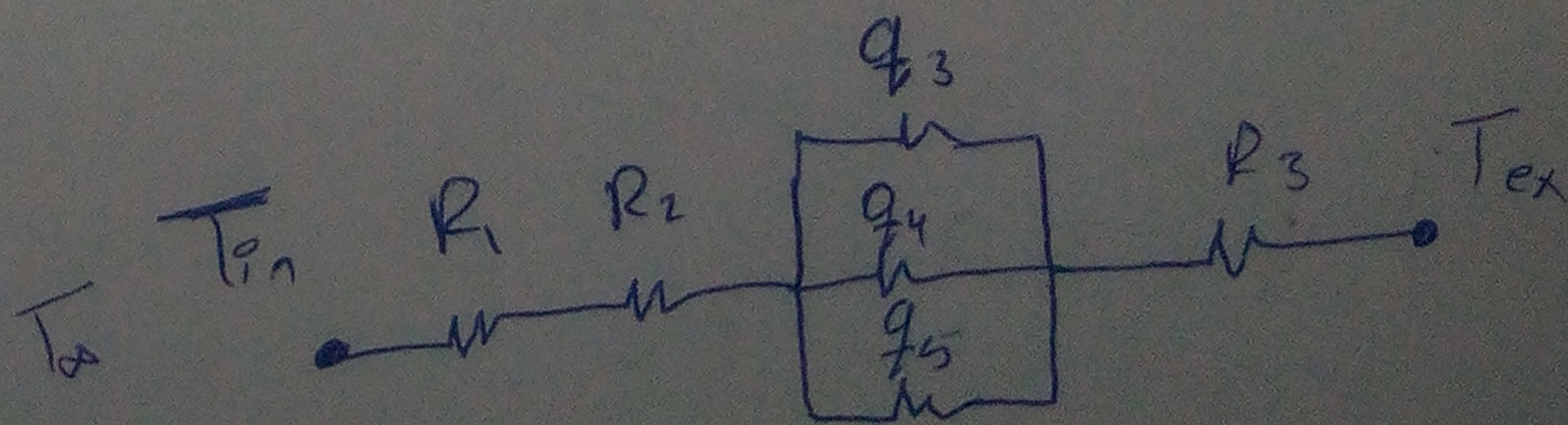
$$R_1 = \frac{L_1}{k_1 A_1} \iff \frac{L}{R} = \frac{KA}{L} \implies q = \frac{\Delta T}{\Sigma R} \iff I = \frac{\Delta U}{\Sigma R}$$

② Convection

$$q_{conv} = hA(T_s - T_\infty)$$

↑  
from table

(convective heat transfer coefficient)





### ③ Radiation

$$q_{\text{rad}} = \epsilon \sigma A (T_1^4 - T_2^4)$$

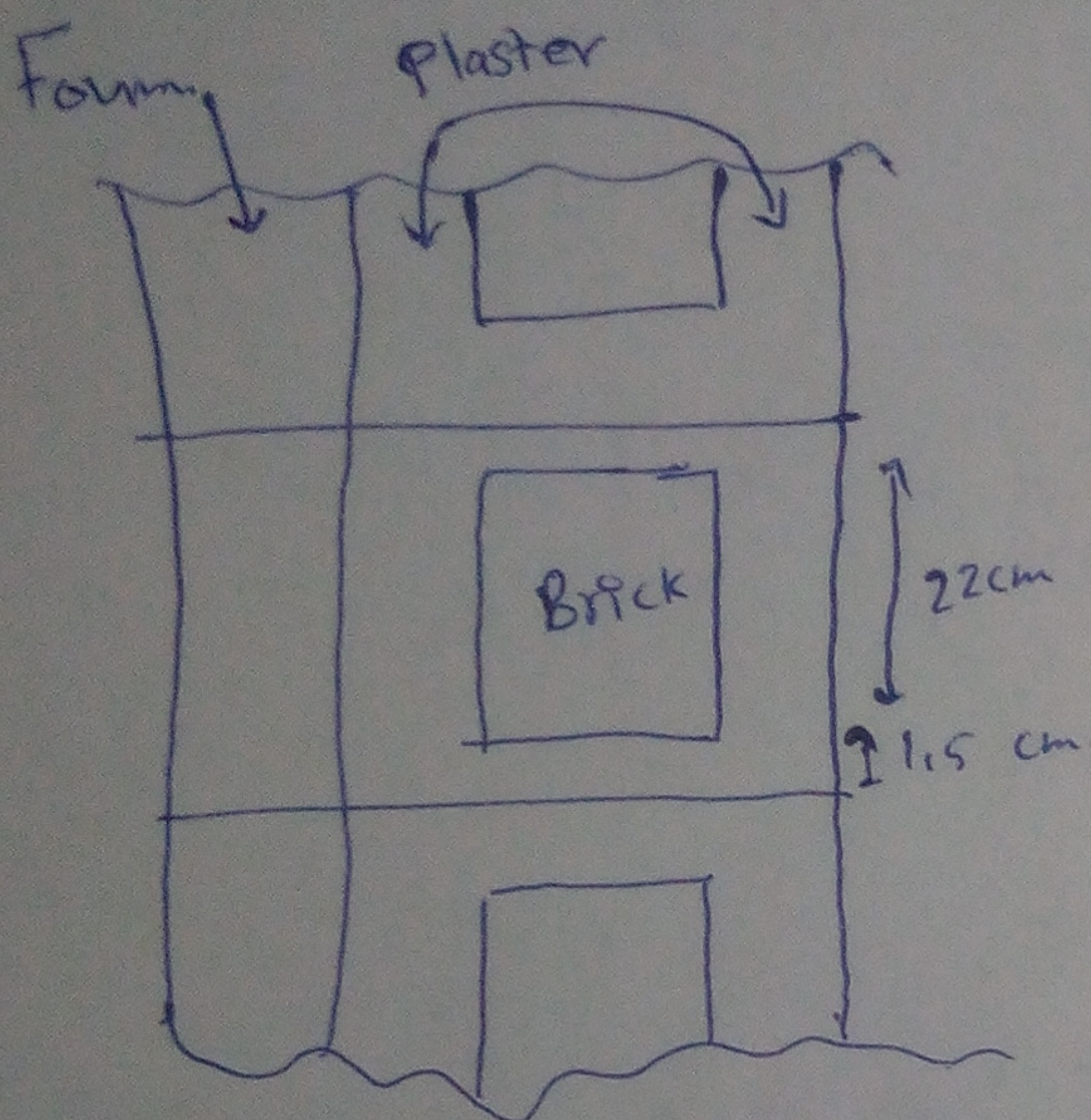
$\epsilon < 1$   
 $\epsilon$ : emissivity  $\epsilon = 1.0$  black body.  
 $\sigma = 5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4$

radius for earth 6,400 km ("

5.8.19

Wall panel

Solve ex 17-6 !



$$R_1 = \frac{L}{h_o A} = \frac{1}{10 \times 0.25} = 0.4 \text{ } ^\circ\text{C/W}$$

$$R_2 = \frac{L_2}{k_2 A_2} = R_{\text{foam}} = \frac{0.03}{(0.026)(0.25)(1)}$$

$$\boxed{R_2 = 4.615 \text{ } ^\circ\text{C/W}}$$

$$R_3 = \frac{L_3}{k_3 A_3} = \frac{0.02}{(0.22)(0.25)} = 0.363 \text{ } ^\circ\text{C/W}$$

$$R_7 = \frac{1}{k_i A} = \frac{1}{25(0.25)} = 0.16 \text{ } ^\circ\text{C/W}$$

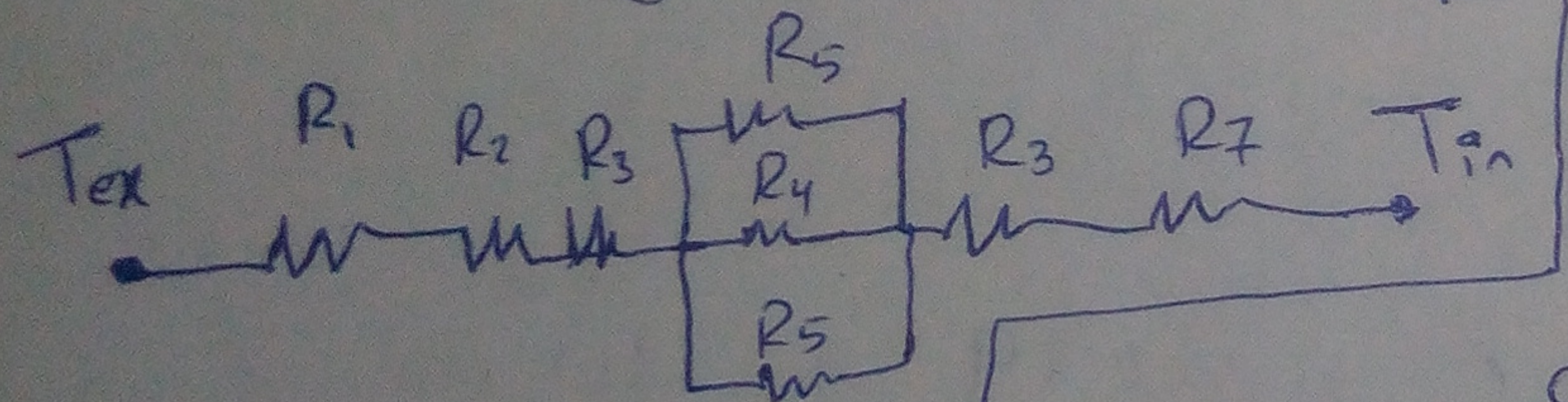
$$\#A = 5 \times 3 = 15 \text{ m}^2$$

$$= 5(0.25 \times 12) = 15$$

$$60 \times (0.25)$$

$$\# \text{Unit area} = 0.25 \text{ m}^2$$

$$Q = \frac{\Delta T}{\Sigma R}$$



$$R_1 = \frac{1}{h_o}$$

$$R_7 = \frac{1}{h_i}$$

$$R_4 = \frac{0.16}{(0.72)(0.22)} = 1.01 \text{ } ^\circ\text{C/W}$$

parallel!

$$R_5 = \frac{0.16}{(0.22)(0.015)} = 48.5 \text{ } ^\circ\text{C/W}$$

$\Delta T(\text{K}) = \Delta T(\text{ } ^\circ\text{C})$

$$\Sigma R_{\text{parallel}} = \frac{1}{\left(\frac{2 \times 1}{48.5} + \frac{1}{1.01}\right)} = 0.96 \text{ } ^\circ\text{C/W}$$

$$\Sigma R = 0.4 + 4.615 + 2(0.363) + (0.96 + 0.16)$$

$$\boxed{\Sigma R = 6.87 \text{ } ^\circ\text{C/W}}$$

$$Q = \frac{\Delta T}{\Sigma R} = \frac{30}{6.87} = 4.36 \text{ W/0.25 m}^2$$

$$\boxed{Q_{\text{tot}} = 262 \text{ W}} \quad \#$$



6.8.19

Cult pur!

## Ch. 18 Lumped Capacitance.

$$\frac{T(t) - T_{\infty}}{T_i - T_{\infty}} = e^{\frac{-t}{\tau}} = e^{-bt}$$

eq. 18.1

$$\tau = \frac{1}{b} = \frac{t}{(F_o \cdot Bi)}$$

$$b = \frac{hA_s}{\rho C_p V} = \frac{Bi \cdot F_o}{t}$$

$$L_c = \frac{V}{A_s}; \quad Bi = \frac{hL_c}{k} = \frac{ht}{A_s k}$$

$$F_o = \frac{\alpha t}{L_c^2}; \quad \alpha = \frac{k}{\rho C_p}$$

the equations are given in final exam!

$$\Rightarrow F_o = \frac{kt}{\rho C_p L_c^2}; \quad Bi = \frac{hL_c}{k}$$

Solve ex 18-1

$$Bi = \frac{hL_c}{k} = \frac{210 \times 0.0005}{3 \times 35} = 0.001 < 0.1$$

$$r = \frac{0.0010}{2}$$

$$L_c = \frac{0.0005}{2} \text{ m.}$$

$$k = 35 \text{ W/m.K}$$

$$\rho = 8500 \text{ kg/m}^3$$

$$C_p = 320 \text{ J/kg.K}$$

$$h = 210 \text{ W/m}^2\text{.K}$$

t = ?

$$F_o = \frac{\alpha t}{L_c^2} = \frac{k}{\rho C_p} \left( \frac{1}{L_c^2} \right) t = \frac{12 \times 10^{-5} t \times 9}{(0.0005)^2} = \frac{10.8 \times 10^{-5} \times 10^8 t}{25}$$

$$\alpha = \frac{h}{\rho C_p} = \frac{35}{8500(320)} = 1.2 \times 10^{-5} \text{ m}^2/\text{s}$$

= 432t

$$b = \frac{1}{\tau}; \quad \tau = \frac{t}{(F_o)} = \frac{k}{(432t)(0.001)} = 23$$

$$-2 \times 2.3 = \ln(0.01) = e^{-(t/23)}$$

$$\frac{99-100}{0-100} = \frac{-1}{-100} = 0.01$$

$$= \frac{-t}{2.3} \rightarrow t = 10.6 \text{ s} \quad \#$$

$$t = 4.6 \text{ s}$$

just for know.



Ch. 10

concepts only!

Ch. 1 + Ch. 2 + Ch. 3

just reading [concepts]

Ch. 11

Imp ex-11.1

problems 5<sup>th</sup> (11-14)

(11-16)

! imp. pr ← (11-49)

Final material ("  
Thermal & Fluid Science.

Good luck 😊

Ch. 12

concepts only

Ch. 13X

Ch. 14

\* examples (1, 3, 6, 8)  
pr pr

\* equation  
(14-44)

\* suggested prob. (43, 73, 97)

Ch. 18

examples (1, 2)

suggested (64)

Ch. 16

concepts only!

Ch. 17

examples (6)  
pr

suggested problems (55, 56, 60)